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## Permanent Magnet Diploes and Quadrupoles for FFAGs

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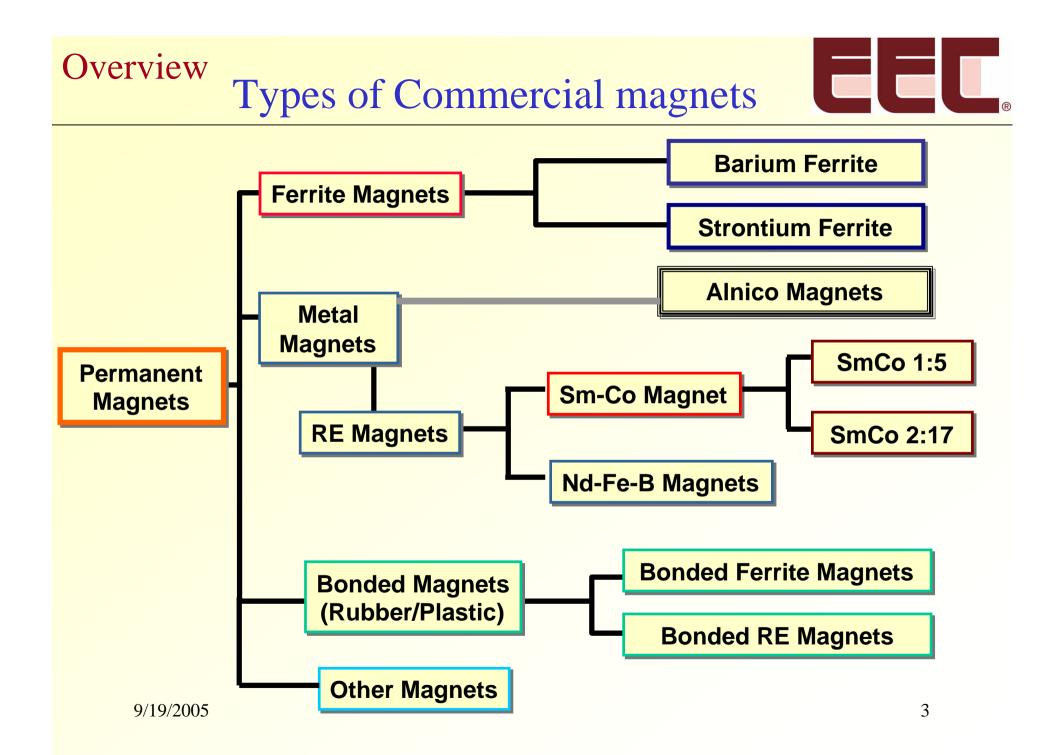
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## Outline



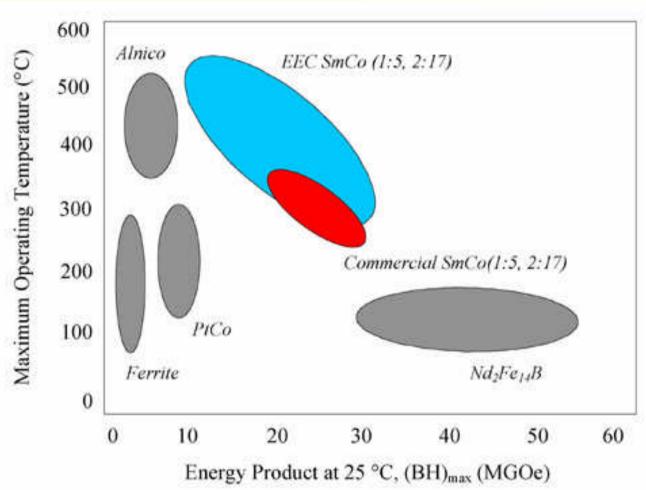
- (1) Permanent Magnet Overview
- (2) Some Design Considerations
- (3) Radiation Effect
- (4) Permanent Magnet Dipoles
- (5) Permanent Magnet Mangles
- (6) Permanent Magnet Quadrupoles
- (7) Summary



#### (BH)<sub>max</sub> versus Maximum Operating Temperature



Overview





Some factors to consider:

- (1) Magnetic performance
- (2) Corrosion resistance
- (3) Thermal stability
- (4) Radiation resistance
- (5) Magnetization direction
- (6) Manufacturability
- (7) Cost



- Typical magnetic properties, in terms of energy product, of selected commercial magnets:
- ✓ Sintered Nd-Fe-B magnets: up to 50 MGOe
- ✓ Sintered Sm-Co magnets: up to 32 MGOe
- ✓ Isotropic bonded Nd-Fe-B magnets: up to 10 MGOe
- ✓ Sintered ceramic magnets: up to 4 MGOe
- ✓ Cast Alnico magnets: up to 9 MGOe

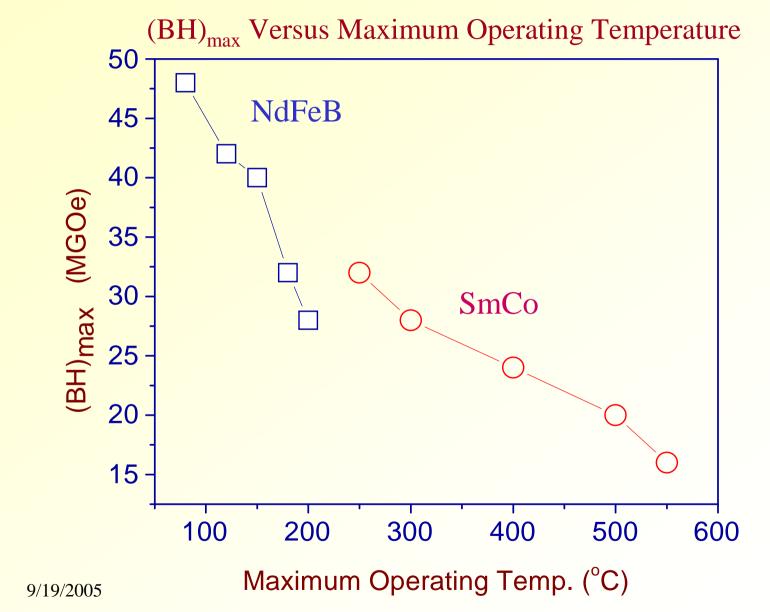


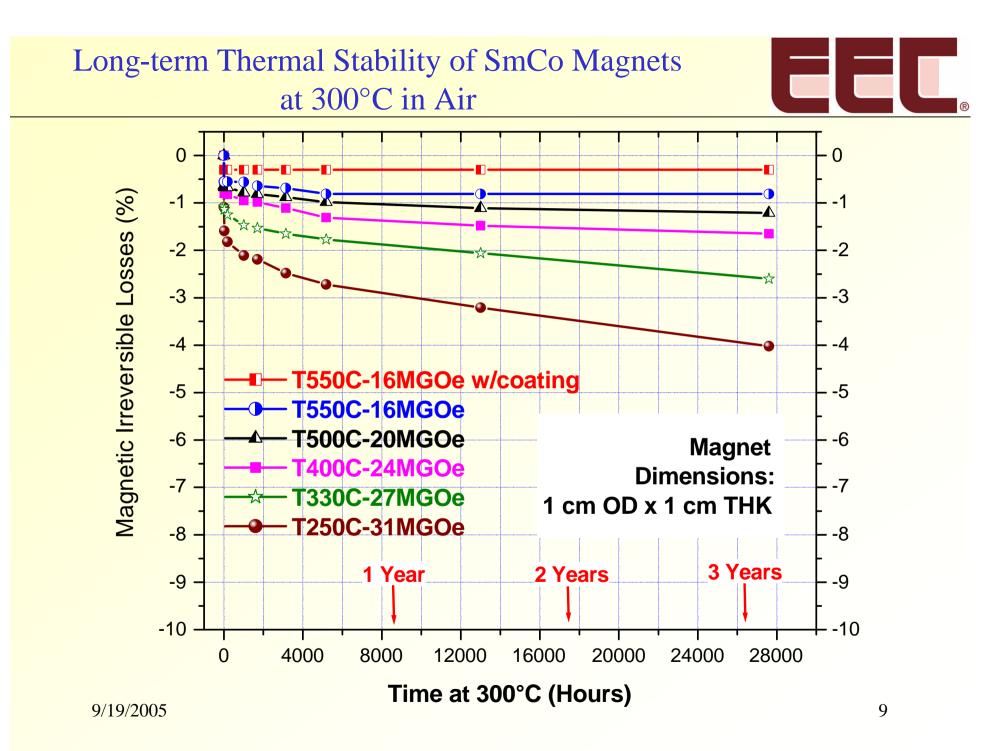
#### **Maximum operating temperature of sintered magnets**

Magnets	Maximum Operating Temp.*
NdFeB with $_{i}H_{c} = 12 \text{ kOe}$	80°C
NdFeB with <sub>i</sub> H <sub>c</sub> =17 kOe	120°C
NdFeB with <sub>i</sub> H <sub>c</sub> =20 kOe	150°C
NdFeB with <sub>i</sub> H <sub>c</sub> =25 kOe	180°C
Conventional SmCo magnets	300°C
EEC24-T400 magnets (patented & a	vailable) 400°C
EEC20-T500 magnets (patented & a	vailable) <b>500°C</b>
EEC16-T550 magnets (patented & av 9/19/2005	vailable) <b>550°C</b>

#### Rare Earth Magnets -- Properties vs. Temperature









High temperature magnets

➢DoD initiated the More Electric Aircraft program, which requires magnets with maximum operating temperature more than 400°C

➢Funded by the Department of Defense, a series of sintered SmCo 2:17 magnets were developed at EEC with maximum operating temperature as high as 550°C

These patented SmCo UHT magnets were introduced to the industry in 1999.



PM Grades	B <sub>r</sub> (kG) (kG)	(BH) <sub>max</sub> (MGOe)	Max. operating temp (°C)
EEC2:17-31	11.6	31	250
EEC2:17-27	10.8	27	300
<b>EEC24-T400</b>	10.2	24.5	400
<b>EEC20-T500</b>	9.3	21	500
<b>EEC16-T550</b>	8.6	17	550



## Nd-Fe-B sintered magnets

#### Key features:

- ≻Highest (BH)<sub>max</sub> available (up to 50 MGOe)
- Less expensive than Sm-Co magnets
- Corrosion resistance is not good
- >Special coating is required
- ➢ Maximum operating temperature is very low compared to SmCo magnets



PM Grades	B <sub>r</sub> (kG) (kG)	(BH) <sub>max</sub> (MGOe)	Max. operating temp (°C)
N50	14-14.5	48-51	70
N45	13.2-13.8	43-46	70
N45M	13.2-13.6	43-46	100
N42SH	12.8-13.2	40-43	120
N33UH	11.3-11.7	31-34	180

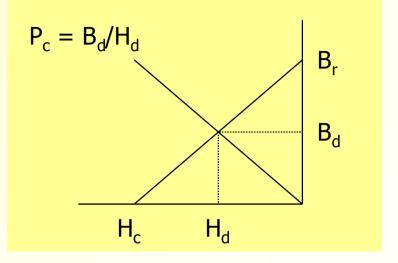
## Some Design Considerations



## Permeance Coefficient P<sub>c</sub>

In the magnetic circuit, a magnet will operate at a specific point on its extrinsic demagnetization curve:

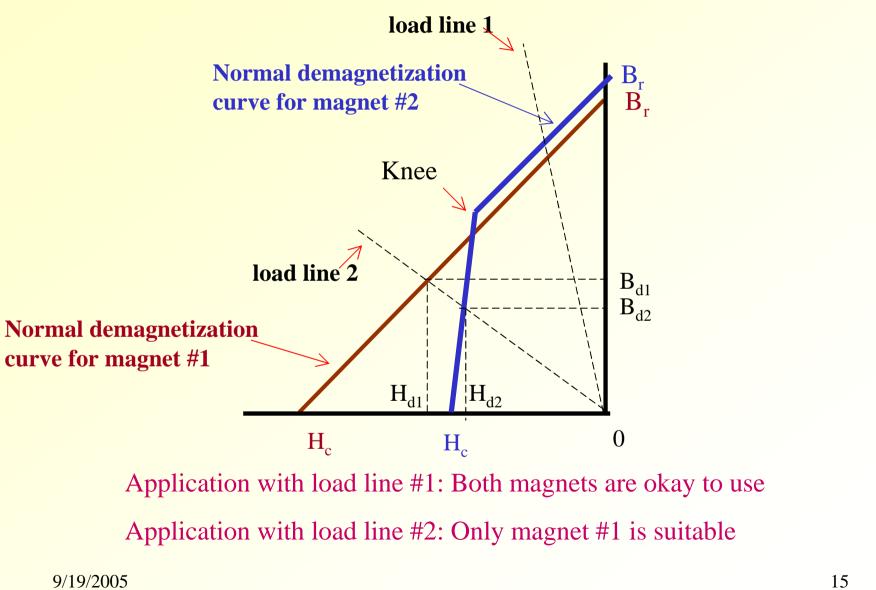
 $P_c = B_d / H_d$ 



#### Also known as **load line** or **operating point**

➢ It is related to the dimensions of the magnets and the associated magnetic circuit

#### Why straight-line demagnetization curves?



#### **Radiation Effect**

The effects of radiation on permanent magnets was studied at EEC under a NASA STTR Contract

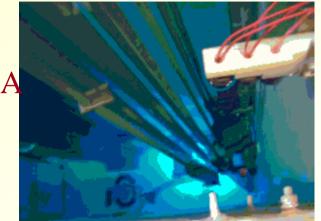
>All Samples have a L/D ratio of 1.25

Permanent Magnets Studied:

✤ EEC T500 and T300 SmCo 2:17 magnets

✤ Nd-Fe-B Magnets

Radiation Source: Ohio State University Research Reactor



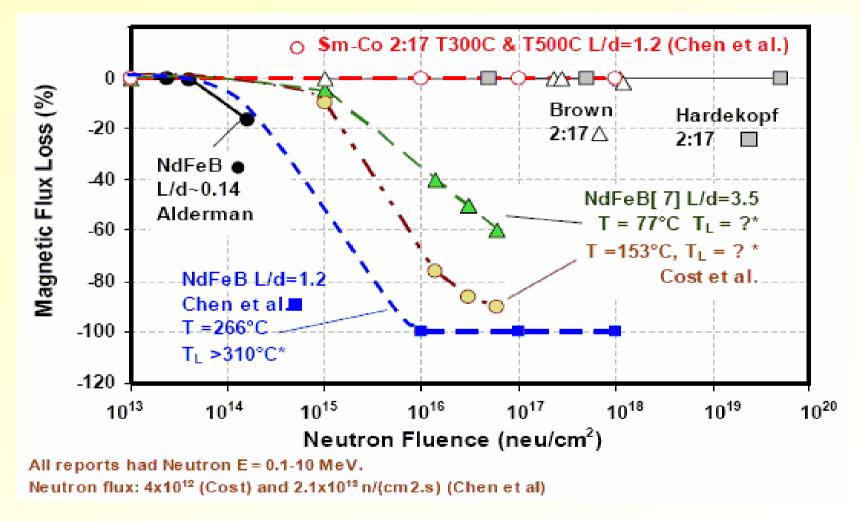
**OSU** Reactor



Samples in quartz tubes

#### Permanent Magnets and Radiation Effect



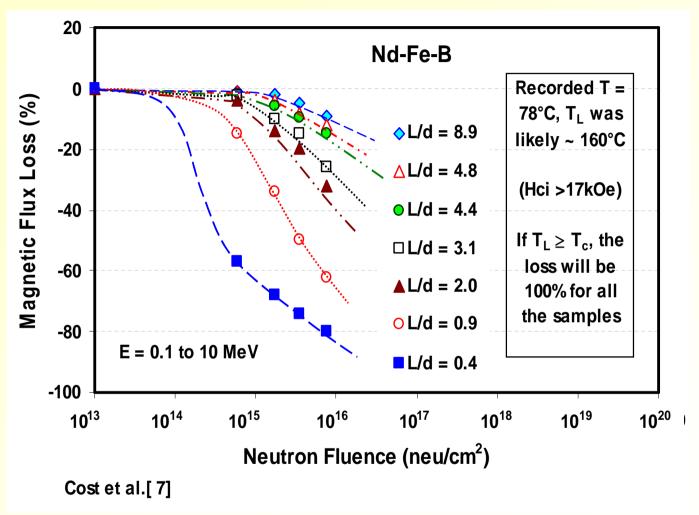


C.H. Chen, J. Talnagi, J.F. Liu, P. Vora, A. Higgins and S. Liu, IEEE Trans. Magn. 41(2005)3832 17

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#### Working Point and Radiation Effect





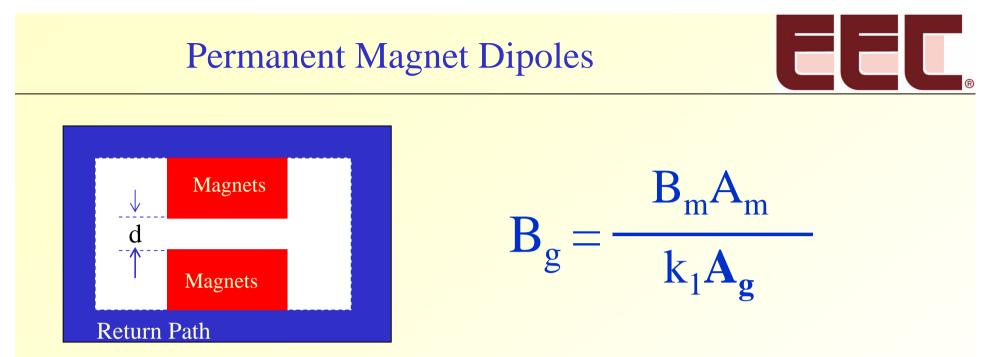
J.R. Cost et al, IEEE Trans. Mag.24 (3), 2016-2018 (1988).

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The major radiation damage is caused by radiationinduced thermal spikes

- The dominant factor for radiation tolerance is thermal stability, which is related to the following factors:
- (1) Curie temperature of permanent magnets
- (2) Working point of permanent magnet in the system
- (3) Intrinsic coercivity



 $A_m$  =Magnet area perpendicular to the direction of magnetization;  $B_m$  =Flux density of the magnet corresponding to the operating point of the demagnetization curve;

 $B_g$  =Flux density desired in the air gap;

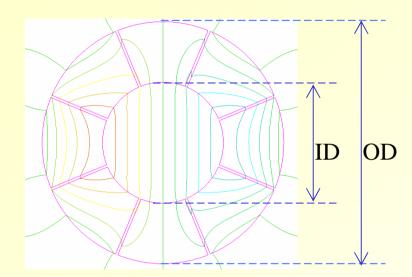
 $A_g$  = Cross section area of the air gap perpendicular to the flux lines.

## The Air Gap Flux Density Is A Lot Lower Than The B<sub>r</sub> Of The Permanent Magnets

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#### Permanent Magnet Dipoles





Halbach PM Dipole Structures:  $B_g = B_r \ln(OD/ID)$ 

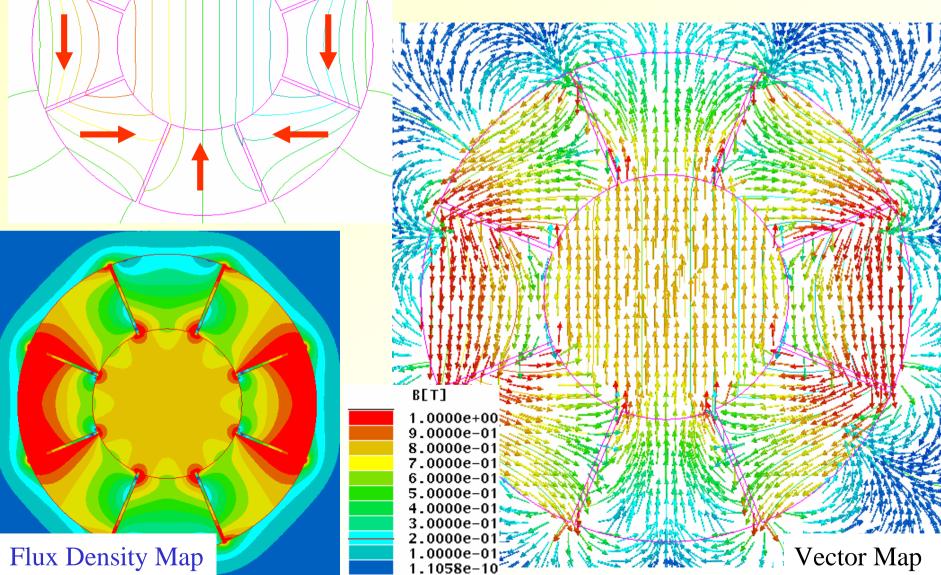
There is no upper limit for air gap flux density in Halbach dipole structures according to above equation. But in reality it would be limited by:

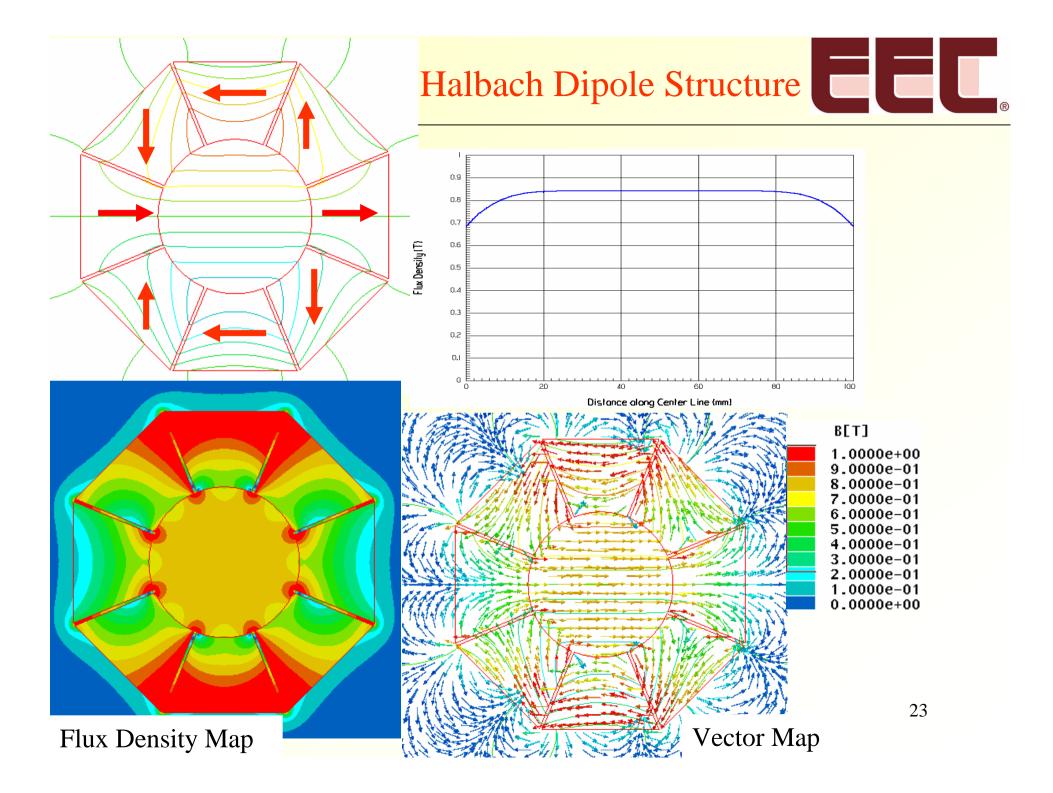
(1) The realistic size

(2) The demagnetization effect



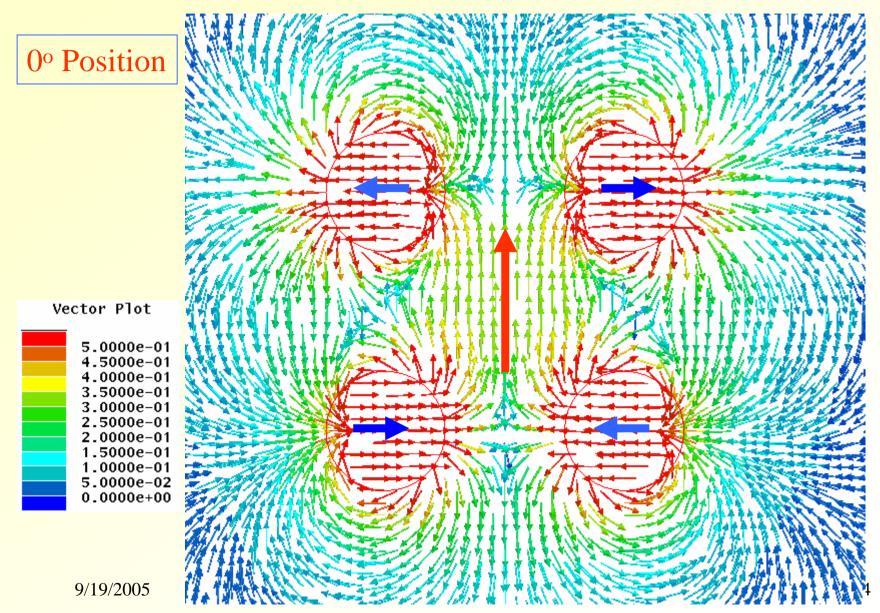
### Halbach Dipole Example

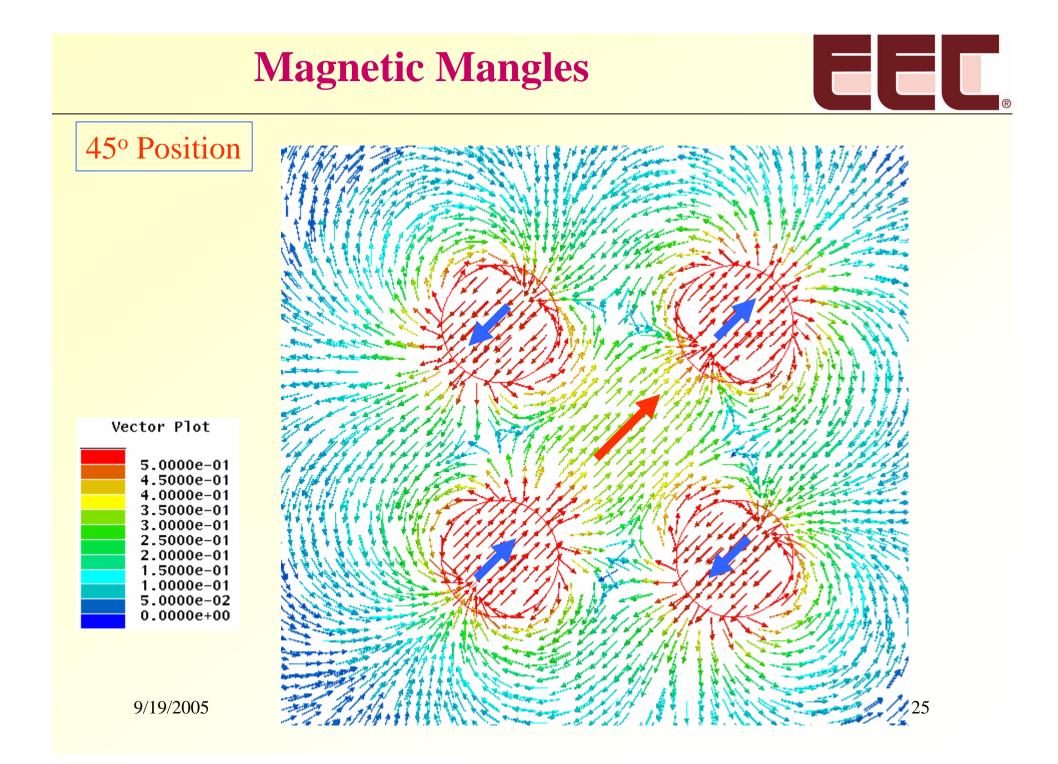






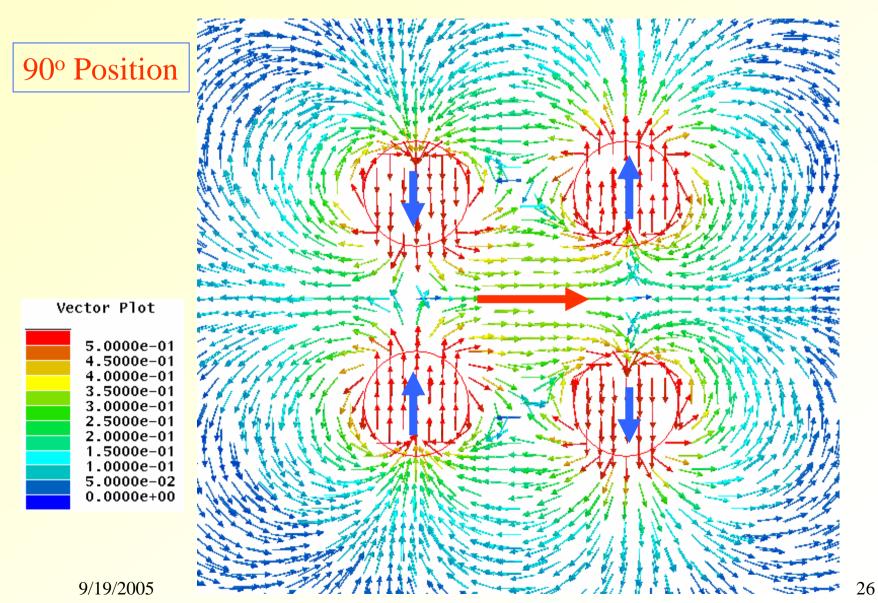
#### **Magnetic Mangles**

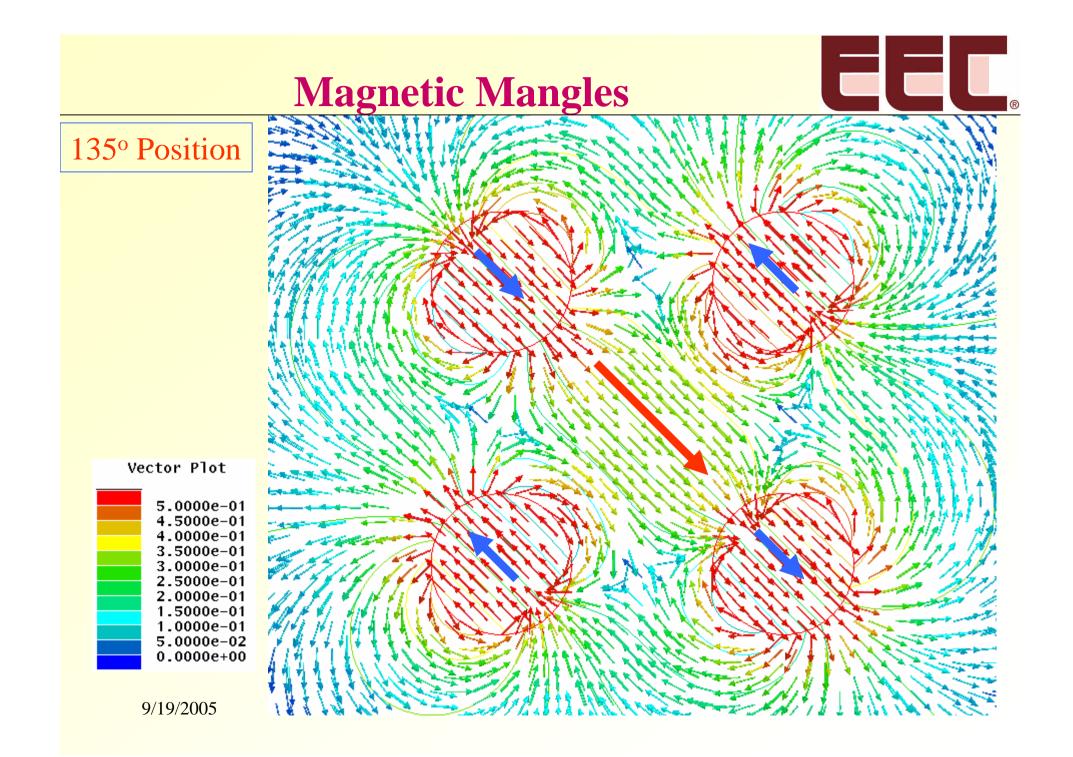






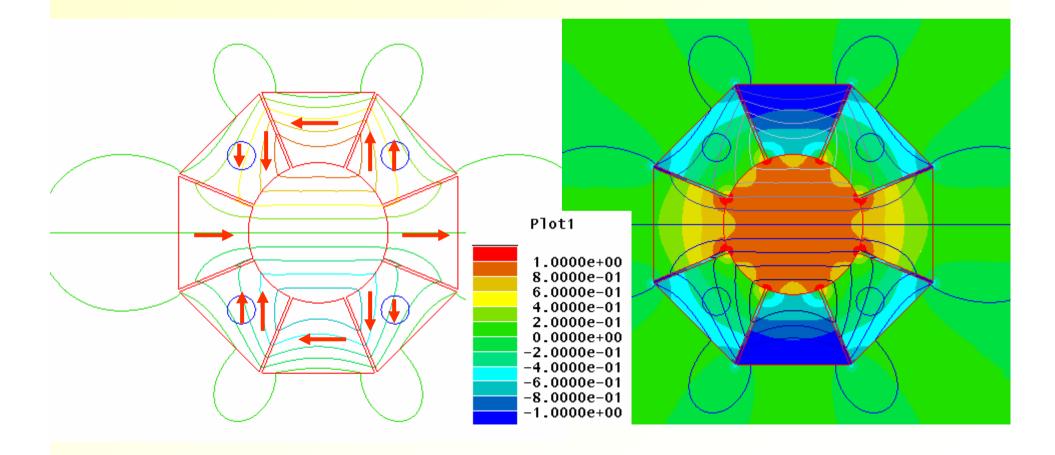
#### **Magnetic Mangles**





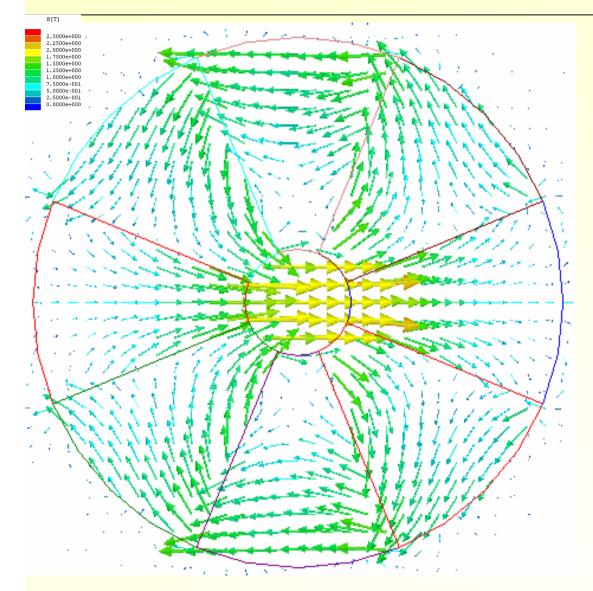


Combination of magnetic mangles and Habach structures can make the air gap flux density adjustable to some degree



#### Halbach Dipole for FFAGs





✓ 4 Tesla PM prototype
Halbach cylinder was
made in Japan.\*

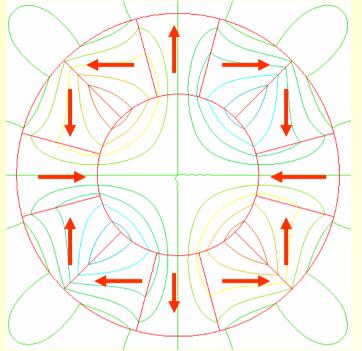
✓ EEC has produced many Halbach structures for a variety of applications.

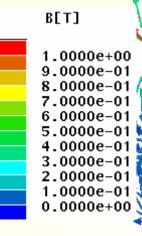
✓ Sintered SmCo or high H<sub>ci</sub>NdFeB magnets are good choices

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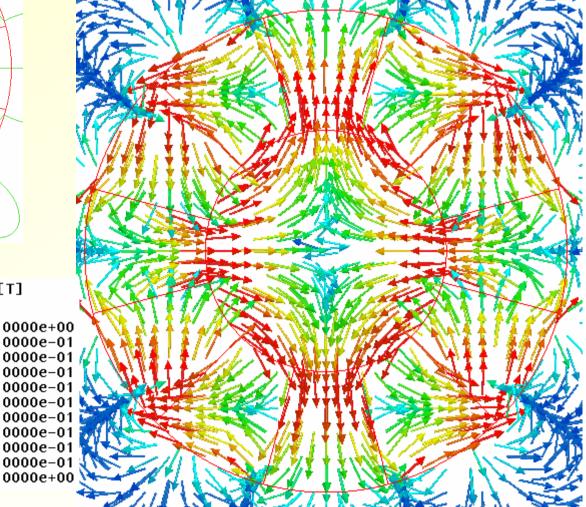
\**M. Kumada et al, PAC2001, 3221.* 

# A Example of Halbach PM Quadrupole

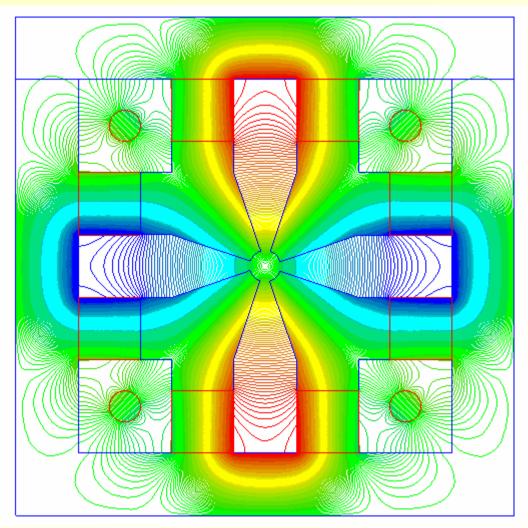




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#### Adjustable Magnetic Quadrupoles



Adjustable magnetic quadrupoles as reported by Fermi lab and SLAC\*:

Diametrically magnetized SmCo 2:17 tuning rods

➤Tuning rods rotation changes the strength of field gradient

\* J. T. Volk et al, PAC2001, p217

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## Summary

✓ Permanent magnet dipoles and quadrupoles can have high air gap flux density if designed with Halbach principles.

✓ Innovative designs can make the air gap flux density adjustable.

✓ Permanent magnet selection might include tradeoffs between cost and performance.

✓ SmCo magnets are far superior to NdFeB magnets with respect to radiation resistance.

## **Contact Information**

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