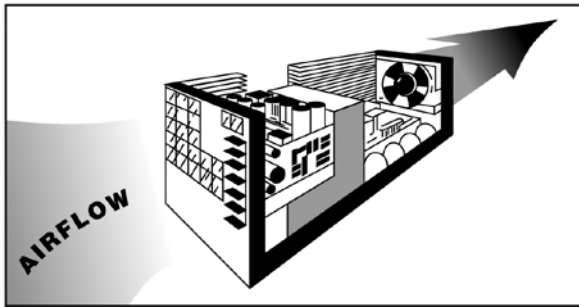


THERMAL DESIGN

The need for forced-air cooling should be determined at an early stage in system design. It is important that the design plans for good airflow to heat-generating components and also allows adequate space and power for the cooling fan.

The first stage in designing a forced-air cooling system is to estimate the required airflow. This depends on the heat generated within the enclosure and the maximum temperature rise permitted.



Enclosure with Cover Removed

The airflow required can be obtained either by calculation or from a graph.

The equation for calculation is:

$$Q_1 = \frac{0.05 H}{\Delta T} \quad Q_2 = \frac{1.76 H}{\Delta T}$$

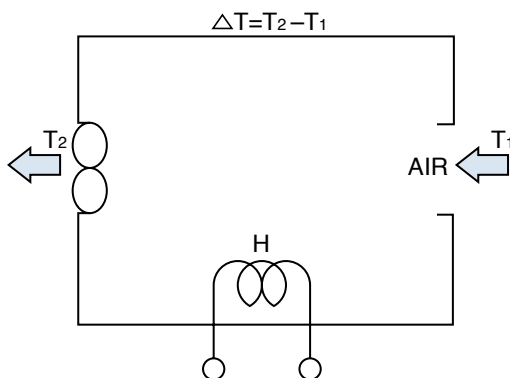
Where:

Q_1 = Airflow required in m³/min

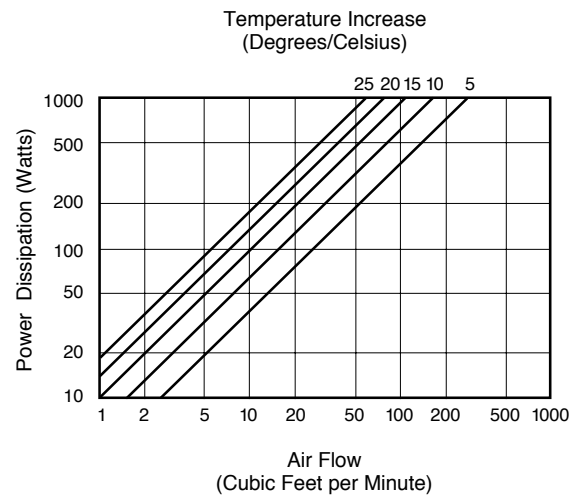
Q_2 = Airflow required in cubic feet/min

H = Heat dissipated in watts

ΔT = Temperature rise above inlet temp °C



In the following graph, the vertical axis represents the heat to be removed and the horizontal axis represents the airflow; both axes are logarithmic. The sloping lines define the temperature rise in °C. To use the graph, find the sloping line that represents the permitted temperature rise. Then, find the point on this line that corresponds to the heat to be removed. The horizontal position of this point shows the airflow required.



Power Dissipation vs. Airflow for Various Temperature Increases

SYSTEM IMPEDANCE & OPERATING POINT

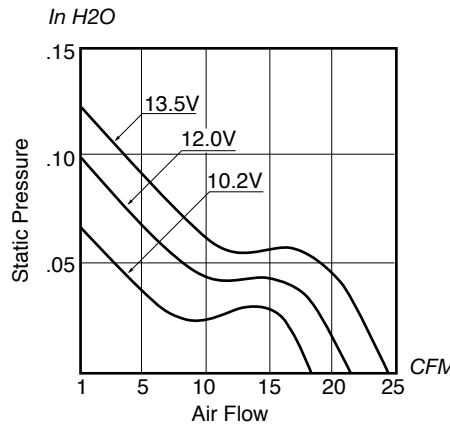
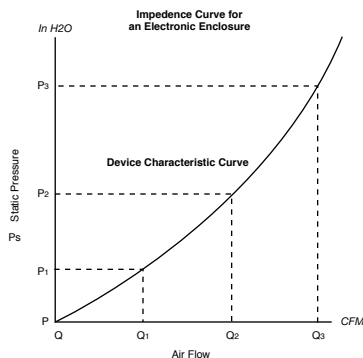
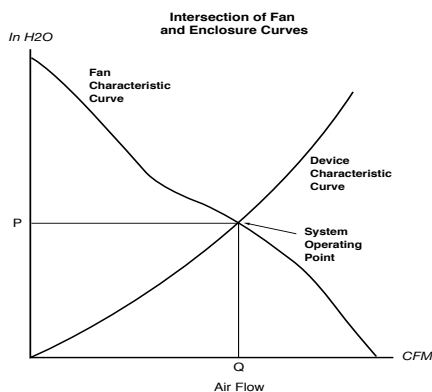
Obstructions in the airflow path cause static pressure within the enclosure. To achieve maximum airflow, obstructions should be minimized. However, obstructions in the form of baffles may be necessary to direct the airflow over the components that need cooling.

Chart 2.1 on the next page illustrates the nonlinear relationship between airflow and static pressure for a typical fan. The System Impedance curve, Chart 2.2, is a property inherent to an individual electronics enclosure. This curve can easily be generated experimentally, by testing the enclosure pressure at various airflow rates. The performance of a fan in a specific application is determined by the intersection of the System Impedance curve and the Fan Characteristic Curve, as shown on Chart 2.3.

SYSTEM IMPEDANCE & OPERATING POINT (continued)

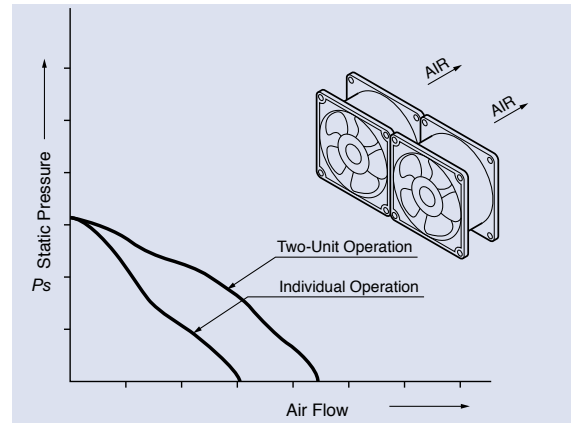
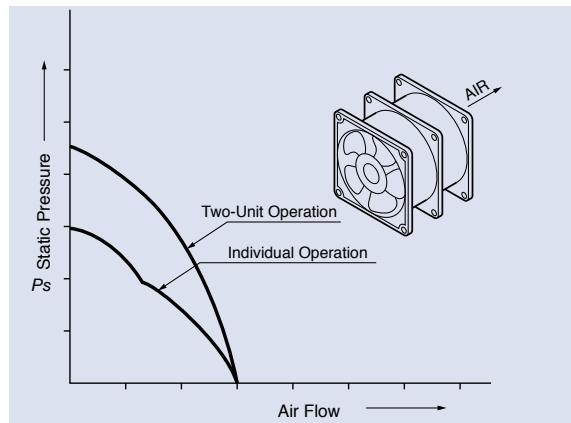
Chart 2.1

Typical relationship between Airflow and Static pressure for an Axial cooling fan.


Chart 2.2

Chart 2.3


MULTIPLE FAN USE

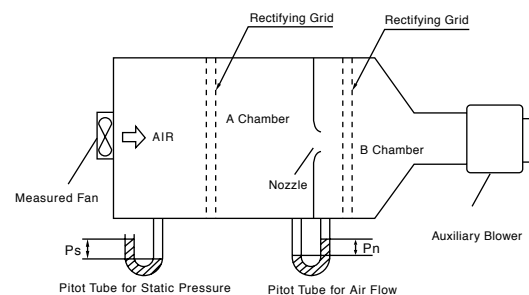
The following figures show the performance characteristics for parallel and series operation of two identical fans.


Parallel Operation

Series Operation

An additional fan in parallel to the first increases airflow in a low static pressure situation. An additional fan in series increases the airflow in a high static-pressure enclosure.

AIRFLOW & PRESSURE MEASUREMENT

An AMCA Standard 210 double chamber is used to accurately measure air volume and static pressure.



AIRFLOW & PRESSURE MEASUREMENT (continued)

Maximum Static Pressure: When the nozzle is closed, the pressure in chamber A will reach maximum.

Maximum Airflow: When opening the nozzle and absorbing the air using the auxiliary blower to make the static pressure zero ($P_s = 0$), the differential pressure (P_n) between A chamber and B chamber will reach maximum. The airflow obtained by applying the differential pressure (P_n) to the above equation can be called the maximum airflow.

Note: Fan performance is calculated using the data obtained from this equipment according to the following formula:

The Equation: Airflow

$$Q = 60 \cdot C \cdot \frac{\pi}{4} \cdot D^2 \sqrt{2g/r \cdot 0.10197 P_n} \text{ (m}^3/\text{min)}$$

C: Coefficient of nozzle air

D: Diameter of nozzle (m)

r: Air density

$$\left(1.293 \times \frac{273}{273+t} \times \frac{P}{1013.25} \right) \text{ (kg/m}^3\text{)}$$

t: Temperature ($^{\circ}\text{C}$)

P: Air pressure (hPa)

P_n : differential pressure of air flow (Pa)

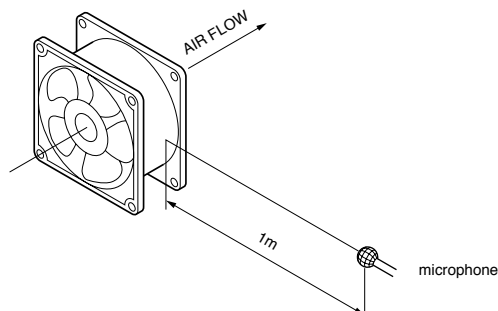
g: 9.8m/s^2

ACOUSTIC NOISE MEASUREMENT

Noise measurements are performed in an Anechoic Chamber with less than 16 dBA background noise in compliance with JIS C 9603 standards.

DC Fan 1 m from inlet side

AC Fan 1 m from the side



FAN SENSORS

Three types of DC fan sensors are available for NMB fans:

Locked Rotor Signal – outputs the status of the fan motor and is ideal for detecting if the fan motor is rotating or stopped.

Tachometer Signal – set to produce two cycles of rectangular waveform as the fan motor makes one rotation and is ideal for detecting speed.

Life Signal – detects a reduction in fan speed at a specified RPM level.

Locked Rotor Alarm Signal:

Output Circuit: Open Collector

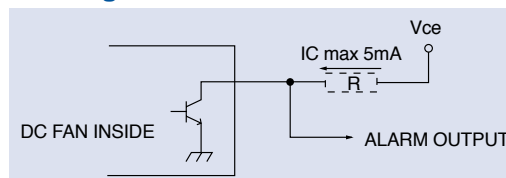
Specifications:

V_{ce} max: +30V

V_{ce} max: +15V (1004KL, 1404KL, 1204KL, 1604KL, 1606KL, 1608KL, 2004KL, 2106KL, 2406KL, BM4515, BM5115, BM5125, BM6015)

I_c max: 5mA ($V_{ce(sat)}$ max = 0.4V)

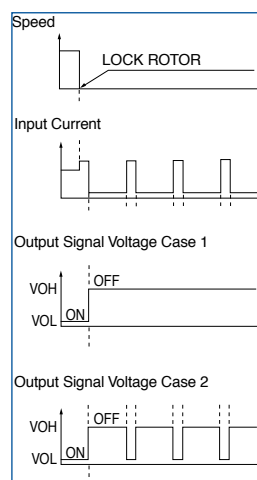
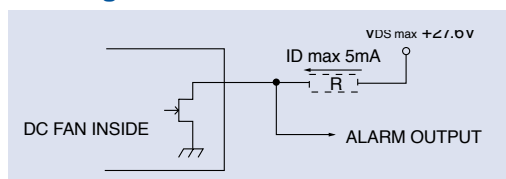
Alarm Signal Circuit



Alarm Signal Output: White, +:Red, -:Black

TTL output is an available option.

Alarm Signal Circuit

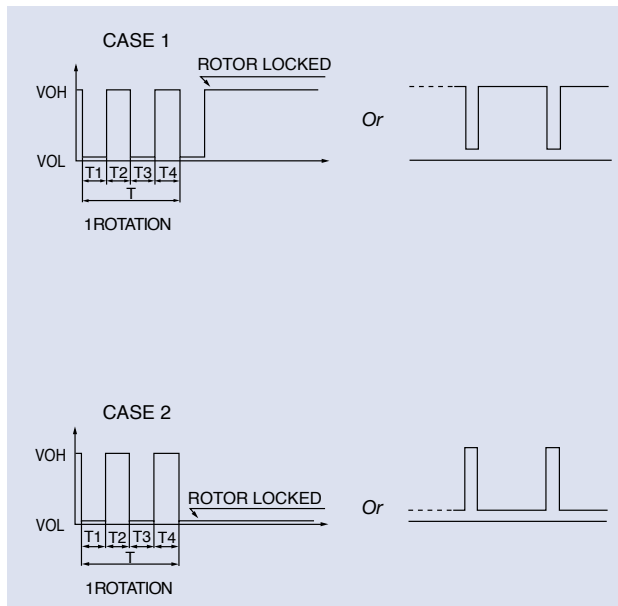


Output Waveform:

At Rated Voltage, the output signal may correspond to either Case 1 or Case 2. Your design should provide for both waveforms.

Tachometer Signal

Output Waveform: At Rated Voltage

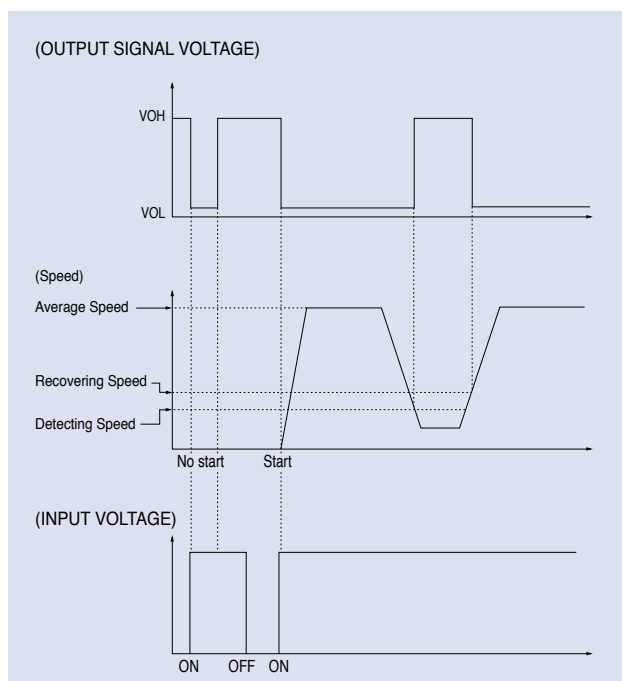


$T = T1 + T2 + T3 + T4 = 1 \text{ Rotation}$, $T1 = T2 = T3 = T4 = 60/4 \text{ m}$
 m: Rotation Speed min^{-1}

The output signal may correspond to Case 1 or Case 2. Your design should provide for both waveforms.

Life Signal

Output Waveform: At Rated Voltage



SPEED CONTROL

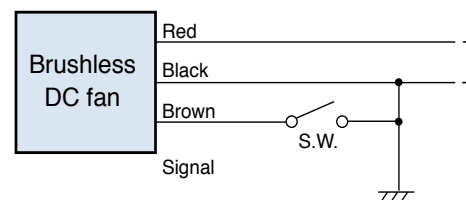
DC fan speed can be controlled in order to optimize cooling, reduce noise and decrease system power draw. There are various methods of controlling fan speed.

2-speed DC fan motor

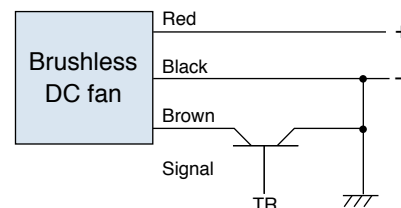
NMB's custom 2 speed fans are available with high and low speeds specified by the customer. The low end operating speed is fixed in order to reduce noise and lower power consumption.

Below is an example of an External connection for a 2-speed DC fan motor.

Control by relay contact



Control by transistor



Switch-over of fan speed

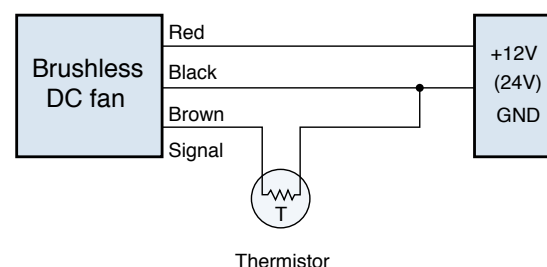
S.W. OFF: LOW SPEED, ON: HI SPEED

Temperature Detecting Variable Speed DC Fan

The RPM may be automatically controlled and synchronized with temperature variation by installing a thermistor.

Varying the control voltage (0 to 6V) enables speed variation between the signal wire and ground.

Example of connection diagram:

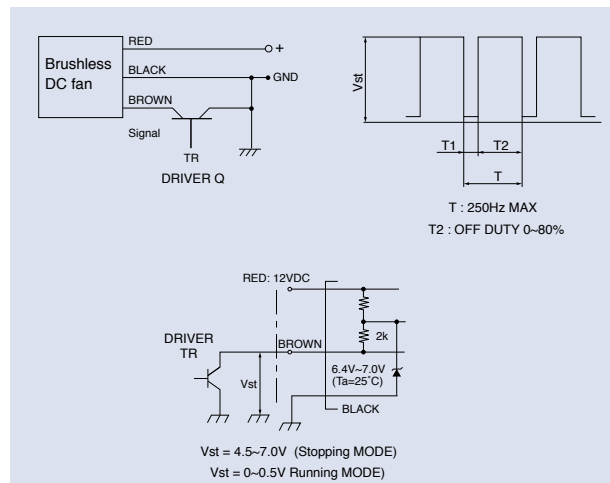


PWM Control DC Fan

In PWM speed control, a fixed frequency square wave is applied to the speed control leadwire of the fan.

The ratio of on time vs. off time (duty cycle) is directly proportional to the speed of the fan.

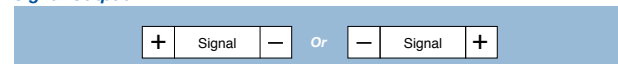
Example:



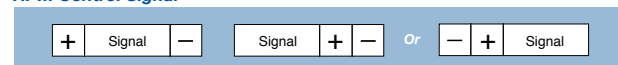
Correct Signal Connection

Correct signal connection is important to prevent damage to the internal fan IC. Connection should be design as shown below:

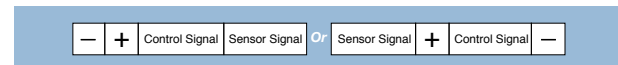
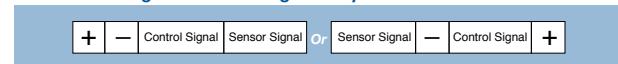
Signal Output



RPM Control Signal



RPM Control Signal & Sensor Signal Output



FAN LAWS

There are various laws useful in determining different fan performance parameters. We have selected a few of these that can be useful in calculating airflow (CFM), pressure (inches H₂O), power consumption (Watts), and noise (dBA), when operating at differing speeds (RPM).

Only fans of the same physical dimensions, same motor and impeller should be used for comparative analysis. The variables below are used in the formulas that follow:

Where:

Speed_k = Known Speed

Speed_n = The new speed we are using for calculation

Airflow_k = Known airflow at Speed_k

Airflow_n = New airflow calculated at new speed

Pressure_k = Known Pressure at Speed_k

Pressure_n = New pressure calculated at new speed

Power_k = Known Power at Speed_k

Power_n = New Power calculated at new speed

Noise_k = Known Noise at Speed_k

Noise_n = New Noise calculated at new speed

Calculating Airflow at different speeds:

$$\text{Airflow}_n = \text{Airflow}_k \left(\frac{\text{Speed}_n}{\text{Speed}_k} \right)$$

Calculating Pressure at different speeds:

$$\text{Pressure}_n = \text{Pressure}_k \left(\frac{\text{Speed}_n}{\text{Speed}_k} \right)^2$$

Calculating Power Draw at different speeds:

$$\text{Power}_n = \text{Power}_k \left(\frac{\text{Speed}_n}{\text{Speed}_k} \right)^3$$

Calculating Noise at different speeds:

$$\text{Noise}_n = \text{Noise}_k + 50 \log \left(\frac{\text{Speed}_n}{\text{Speed}_k} \right)^2$$

Airflow Calculation Example:

If a fan provides 210 CFM of airflow at 3000 RPM. What airflow (CFM) would be expected if the speed (RPM) is increased to 3500 RPM?

Speed_k = 3000 RPM

Airflow_k = 210 FM

Speed_n = 3500 RPM

$$\text{Airflow}_n = \text{Airflow}_k \left(\frac{\text{Speed}_n}{\text{Speed}_k} \right)$$

Airflow_n = 245 CFM

Pressure Calculation Example:

In the example above the fan provides 0.1 inches of H₂O Pressure at the system operating point. What pressure would be expected if the fan speed were increased to 3500 RPM?

Speed_k = 3000 RPM

Speed_n = 3500 RPM

Pressure_k = 0.1 in H₂O

$$\text{Pressure}_n = \text{Pressure}_k \left(\frac{\text{Speed}_n}{\text{Speed}_k} \right)^2$$

Pressure_k = 0.136 in H₂O

Power Calculation Example:

The fan in question draws 22 Watts at 3000 RPM. What power draw would be expected if the fan speed were increased to 3500 RPM?

Speed_k = 3000 RPM

Speed_n = 3500 RPM

Power_k = 22 watt

$$\text{Power}_n = \text{Power}_k \left(\frac{\text{Speed}_n}{\text{Speed}_k} \right)^3$$

Power_n = 34.935 watt

Noise Calculation Example:

The fan in question generates 58 dBA of noise measured 1 meter from the inlet side of the fan. What would the increase in noise be if the the speed were increased form 3000 RPM to 3500 RPM?

Speed_k = 3000 RPM

Speed_n = 3500 RPM

Noise_k = 58 dBA

$$\text{Noise}_n = \text{Noise}_k \left(\frac{\text{Speed}_n}{\text{Speed}_k} \right)$$

Noise_n = 61.347 dBA

NMB TECHNICAL SUPPORT

NMB offers a full range of application and design support services, including thermal modeling and flow analysis. For assistance with any technical issue, please contact the NMB Fan Team through our web site at www.nmbtc.com or e-mail us at fans@nmbtc.com.

UNITS OF MEASURE AND CONVERSIONS

Fan airflow, static pressure, temperature, and dimensions are often referred to in a variety of unit measures. Below are the measures and methods of conversion.

Airflow

CFM	m ³ /min	m ³ /hr	L/sec
1	0.028	1.7	0.47
35.3	1	60	16.7
0.59	0.017	1	0.28
2.12	0.06	3.6	1

Example: To convert from CFM to m³/hr, multiply by 1.7

Static Pressure

in H ₂ O	mm H ₂ O	Pa
1	25.4	249
0.039	1	9.81
0.004	0.1	1

To convert PA to H₂O, multiply by 0.004

Temperature

Degree F = 9/5 C + 32

Degree K = C = 273/15

Linear Dimensions

1mm = 0.0394" ~ 0.04

1" = 25.4mm = 2.54 cm

1U = 44.4 mm = 1.75"

FAN LIFE AND RELIABILITY

Fan Life Testing

Life expectancy of a cooling fan is a critical element in thermal design. NMB uses parametric failure modes during life testing to calculate for life expectancy. Speed (RPM) and Current (mA) failures include both “hard failures” (where the fan is non-functional) and “parametric failures”. These parametric failures are defined as 15% decrease in RPM and an increase in mA of 15%.

Including parametric failure modes leads to a more conservative L-10 and MTTF reporting standard than those methods that measure life performance using only hard failures.

The benefit to the customer is a fan that sets the quality and reliability standard for the cooling industry.

NMB evaluates fan life and reliability during the design phase using accelerated life testing in conjunction with ORT (Ongoing Reliability Testing). Accelerated life testing is used to compress the amount of time required to conduct life testing. Development testing occurs early in the product design, prior to product release. It is vital to characterize the reliability of the product in the initial stages of design to allow for improvements and to meet the reliability specifications prior to release to manufacturing.

Once the design has been through design verification testing and is turned over to manufacturing, ORT is conducted. For some models, ORT evaluation has continued beyond 10 years. The value of ORT is a continued refinement of the accuracy of the accelerated life testing and constant review of the design of the fan. This continued process improvement allows for ongoing evaluation and increase in fan life and reliability.

Under accelerated life testing NMB fans are tested at extreme environmental conditions, with temperature stress factors above standard operating levels. In order to gather meaningful data within a reasonable time frame, the stress factors must be accelerated to simulate different operating environments. High temperature stress is the most common stress factor used for these purposes.

Proper understanding of accelerating stresses and design limits are necessary to implement a meaningful accelerated reliability test. NMB uses the Arrhenius model for determining acceleration factors (AF) during life testing. This is the most commonly used model in accelerated life testing where thermal stress is the primary factor affecting life.

Life test data gathered from different types of fans and blowers lends to highly accurate statistical analysis. This data can produce very detailed information about the behavior of the product for reliability and prediction of fan performance in the field. The Weibull Distribution is a typical method employed by NMB for statistical analysis. An explanation of this calculation model is shown below.

Arrhenius Weibull Model:

Life Stress Relation: Arrhenius

The Arrhenius life-stress relationship is given by:

$$\eta = L(V) = C \cdot e^{\frac{\beta}{V}}$$

Where:

- L represents a quantifiable life measure, which is the scale parameter or characteristic life of the Weibull Distribution.
- V represents the stress level (formulated for temperature and temperature values in absolute units, i.e. degrees Kelvin or degrees Rankine)
- C is one of the model parameters to be determined (C > 0).
- B is another model parameter to be determined

Mean Life or MTTF

The mean, \bar{T} , also called MTTF or Mean Time To Failure, of the Arrhenius-Weibull relationship is given by:

$$\bar{T} = C \cdot \frac{B}{eV} \cdot T \left(\frac{1}{\beta} + 1 \right)$$

Reliable Life

The Arrhenius Weibull Distribution model predicts the length of time at which a defined percentage of a product population will still be operating without failing to meet pre-set criteria. For cooling fans, this is normally characterized as L10 life expectancy, or the time at which 10% of a population will have failed and 90% of a population will continue to operate within specifications.

For the Arrhenius-Weibull relationship, the reliable life, T_R , of a unit for a specified reliability and starting the mission at age zero is given by:

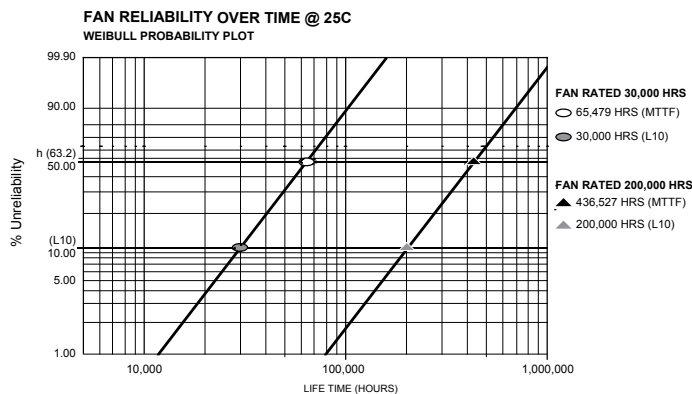
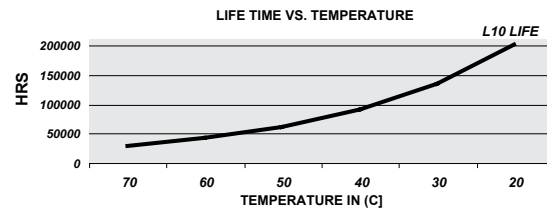
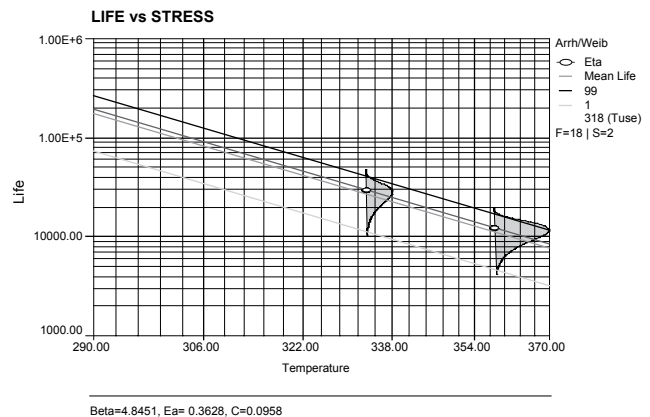
$$T_R = C \cdot \frac{B}{eV} \{-\ln[R(T_R, V)]\}^{\frac{1}{\beta}}$$

This is the life for which the unit will function successfully with a reliability of $R(T_R)$. If $R(T_R) = 0.90$ then $T_R = 90\%$ reliability or 10% unreliability (L10) or the life by which 90% of the units will survive.

NMB uses parametric failure modes, or the condition at which a performance parameter fails to meet pre-set criteria, to record failures during accelerated life testing. This produces a more accurate prediction of field reliability than methods which use only non-operating failure modes to record failures.

Example: Life Experiment Data Using Arrhenius Weibull

Product L10 life expectancy for NMB fans ranges from 30,000 hours to 200,000 hours of continuous operation at room temperature depending on fan speed, frame size, design structure, size of ball bearings and the type of ball bearings used. NMB, a world leader in miniature precision ball bearings design and manufacturing, uses high quality, long life bearings produced in house to ensure extended fan life.



$\beta_1=2.50, \eta_1=73798.94$

$\beta_2=2.50, \eta_2=491992.91$

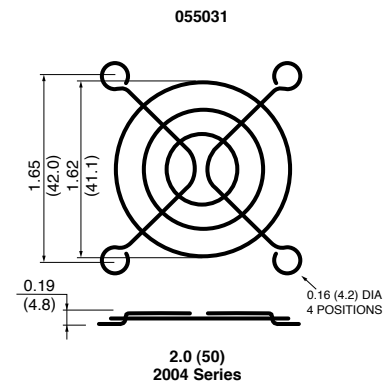
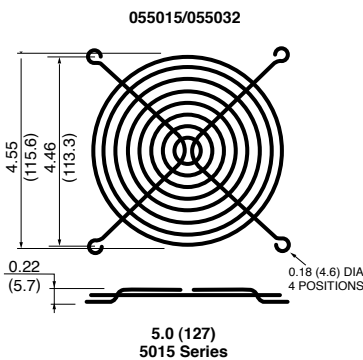
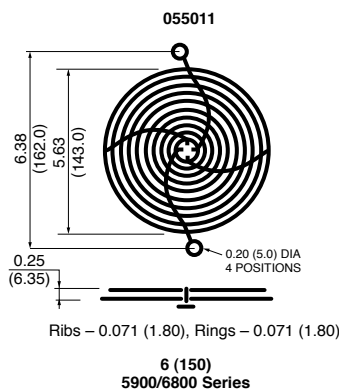
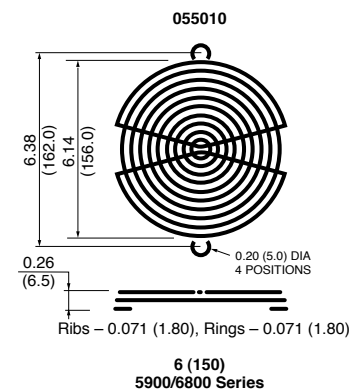
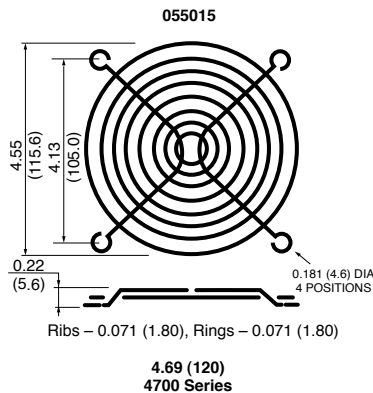
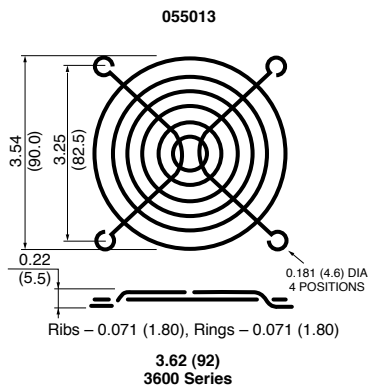
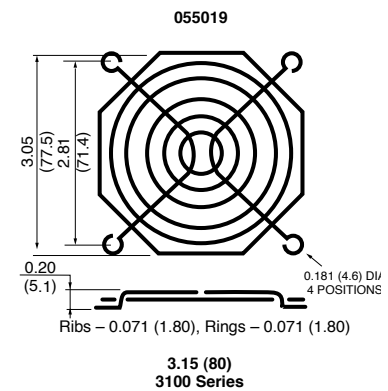
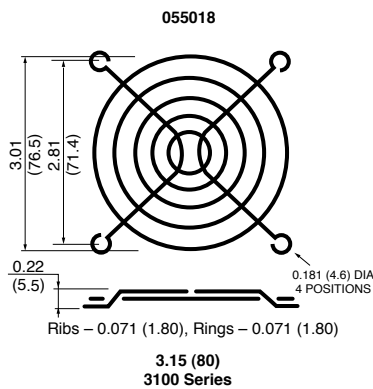
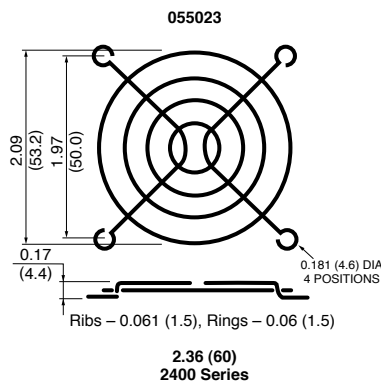
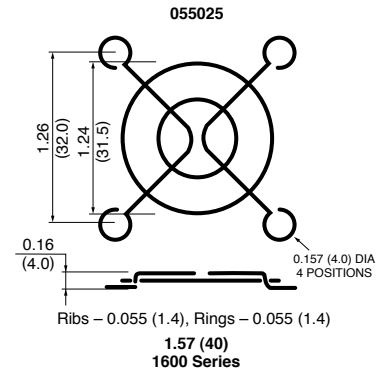
L10 - (10% Unreliability or 90% Reliability Over Time)

MTTF - (Mean Time To Failure or Mean Life)

For specific product life and reliability, please contact NMB's Applications Engineers.

Fan Guards

- Designed to insure safety
- Plating bright nickel chrome, black electro deposit available
- Plating thickness of .0005 min.
- Weld joints withstand 230 lbs. separation force
- Wire base C1010 steel



Fan Guards/Mounting Clips/Cord Sets

Fan Mode	Fan Guards Part Number								Mounting Clips Part Number			Cord Sets Part Number				
	055010	055011	055013	055015	055018	055019	055023	055025	055031	055032	512011	512020	512023	432000	432002	432021
1004KL																
1204KL																
1404KL																
1604KL																
1606KL																
1608KL																
2004KL																
2106KL																
2406KL																
2408NL																
2410ML																
2410ML Vented																
3108NL																
3110KL																
3112KL																
3610KL																
3610KL Vented																
3612KL																
3615KL																
4710KL																
4712KL																
4715KL																
4715SL																
5015KL																
5020KL																
5910PL																
5920PL																
6820PL																
2412PS																
3110PS																
3115FS																
3115PS																
3610PS																
4710PS																
4715FS																
4715MS																
5915PC																

NMB Fan Warranty Policy

NMB warrants our fans to be free from defects in material and workmanship for a period of one (1) year. In order to accommodate transportation and installation we extend this warranty to 15 months from the date of manufacture.

This warranty applies to fans and blowers which are used within the design parameters and when used in an approved application. If there are any questions regarding proper application please contact your NMB representative and an applications engineer can review the customer's operational requirements.

Warranty Limitations and Liability

In the event of an operational failure of an NMB fan or blower, which was used in a manner specifically approved by NMB, NMB will at its option, repair or replace the defective fan or blower with an identical or functionally equivalent product.

In no case will NMB's liability exceed the purchase price of the defective product.

Errors

All information, data and dimension tables in this catalog have been carefully compiled and thoroughly checked. However, no responsibility for possible errors or omissions can be assumed.

Changes

The company reserves the right to change specifications and other information included in this catalog without notice.

Additional Products From NMB

Small Motors

NMB's small motor products include a line of hybrid and permanent magnet stepper motors, as well as NMB's brush and brushless DC motors. The brush DC motor line is ideal for applications that require small size and excellent power output. The brushless DC line is perfect for applications where

Mechanical Bearing Assemblies

NMB's Miniature Precision Ball Bearings are the first component of a highly successful design of a mechanical bearing assembly. Machined components such as magnets, gears, molded and machine plastic parts, die cast parts and special materials are



the environment is sensitive to interference, battery powered equipment and clean room. Standard NMB hybrid and permanent magnet stepper motors are available, as well as many customizable features for your unique application.

For more information on our motor products, e-mail us at: motors@nmbtc.com

Miniature Precision Bearings

Our miniature bearings range in sizes from .1181 to 1.000 inch O.D. (3mm to 26mm), and are available in inch and metric sizes. Stainless steel or chrome steel bearings are available with crown or ribbon type metallic cages, as well as plastic crown type cages. NMB bearings are found in medical equipment, advanced automotive applications and household electrical appliances such as air conditioners, vacuum cleaners, VCRs and video cameras, and in motors for electronic controls systems, among others.

For more information on our miniature bearings, e-mail us at: bearings@nmbtc.com

designed and manufactured to work precisely with NMB precision ball bearings. Complex mechanical bearing assemblies are custom made to your design specifications, and are ideal for medical, office automation, and currency machines, as well as factory and lab automation applications.

For more information on our mechanical assembly products, e-mail us at: assemblies@nmbtc.com

Fan Trays

NMB's extensive selection of AC and DC cooling fans, as well as the latest range of high efficiency motorized impellers are your turn-key solution for your custom fan tray designs. NMB's fan tray product offerings include single or multiple devices, redundant and single-point of failure proof design, intelligent and self regulated control functions, two way communication with system for remote access and wide voltage range design.

For more information on our custom fan trays e-mail us at: info@nmbtc.com





ISO 14001 • ISO 9001:2008 • TS 16949 • OHSAS 18001

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