



Using Large-Signal Measurements for Transistor Characterization and Model Verification in a Device Modeling Program

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- Introduction
- Large-signal measurement data in a device modeling program

- Example: IC-CAP

• Transistor characterization

- Example: MOSFET

Model verification

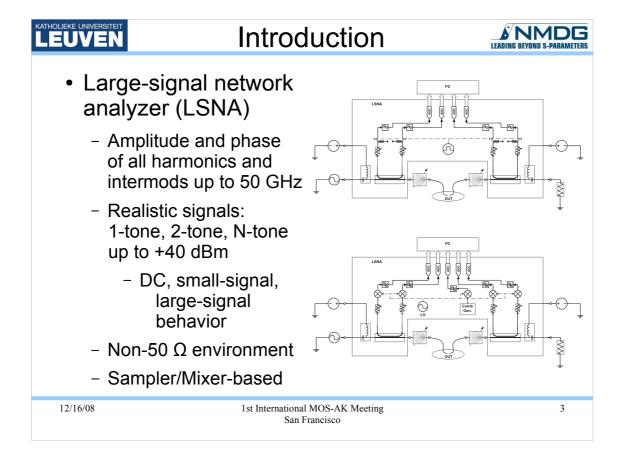
- Example: Angelov model

- Results
- Conclusions

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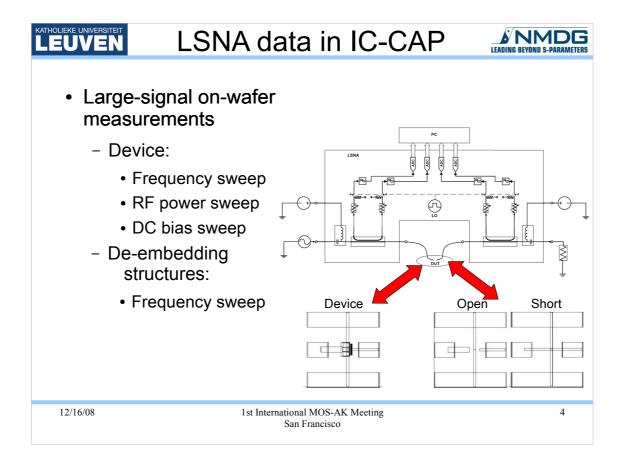
LSNA provides accurate complex values of the incident and scattered traveling voltage waves present at the ports of a 2-port DUT. Harmonic frequency components and intermodulation distortion products are measured in a wide frequency band, even up to 50 GHz.

The measured data give complete information about the behavior of the DUT under realistic signal conditions. The accepted excitations include: one-tone CW signal, two-tone signal, multi-tone signals (periodically modulated signals) with the input powers reaching +40 dBm.

With a single connection of the DUT DC, small- and large-signal behavior can be measured.

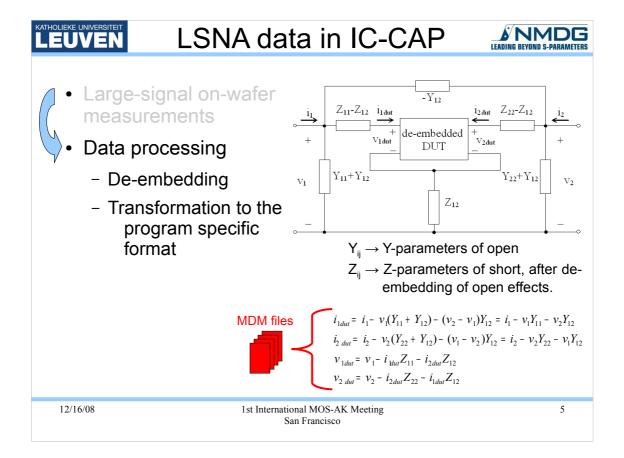
LSNA systems are adapted to work in non-50 Ohm environment (see impedance tuners at the input and output of the DUT).

There are sampler and mixer-based LSNA setups (see the diagrams). In the sampler-based solution, all the frequency components are obtained during one measurements cycle. The data are available faster but the dynamic range is lower than in the second type of systems. In the mixer-based solution, the frequency is swept over the required range and a number of measurements is taken each at different frequency.

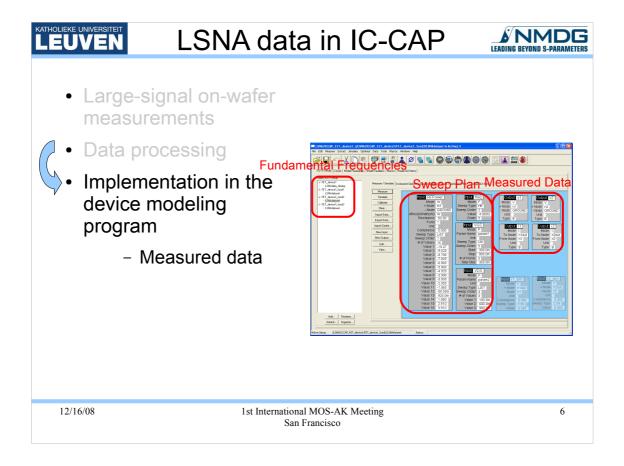


Here, we give an outline of the procedure implementing large-signal measurements in the device modeling program, using as an example Agilent's IC-CAP.

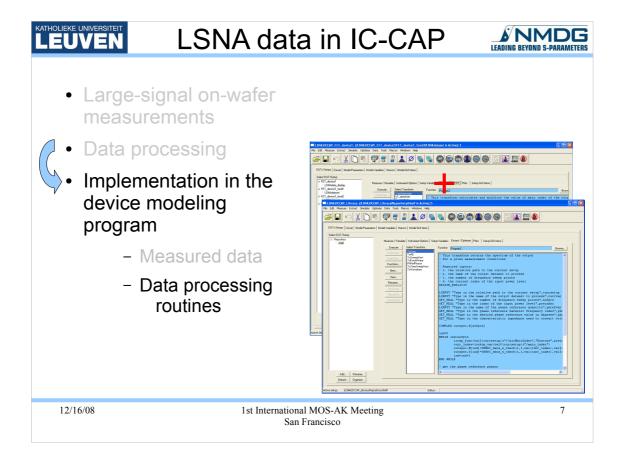
- 1. Perform the LSNA measurements of the on-wafer DUTs:
- a) In case of a transistor, we usually sweep the parameters like the fundamental frequency of the CW signal, the RF input power level, and the DC bias conditions.
- b) In case the de-embedding structures are available (usually open and short dummy structures), only the S-parameter measurements are necessary at the harmonic frequency grid.



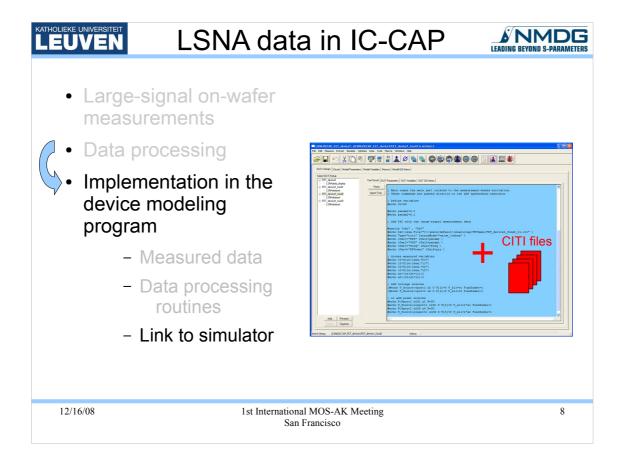
- 2. The next step of the procedure involves the measured data processing:
- a) De-embedding is performed to remove form the large-signal current and voltage spectra the parasitic effects of contact pads and signal path between the probe tips and the device itself. A possible equivalent circuit representation of these parasitics is shown in the figure. The parallel parasitic admittances, mostly due to the contact pads, are identified from the small-signal measurements of the open dummy structure. The impedances of the presented equivalent circuit are obtained from the measured short dummy structure after de-embedding contact pads effects. Finally, the admittances and impedances are de-embedded from the large-signal currents and voltages in frequency domain, as shown in the equations.
- b) The resulting the data is converted to a format readable in the device modeling program. In case of IC-CAP, this is .MDM file format.



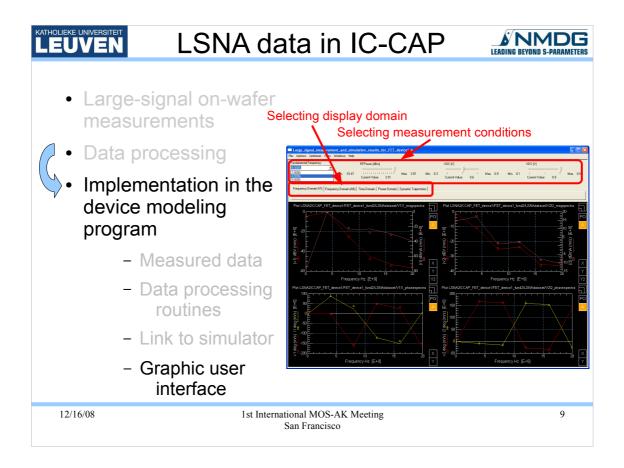
- 3. Finally, the large-signal data can be implemented in the device modeling software.
- a) The (de-embedded) measurements are imported to the environment. In IC-CAP, we can see the sweep parameters as the inputs and the measurements as the inputs. On the presented figure two inputs are grayed out, because they are added to properly store simulated currents later on.
- b) For the maximum usability of the measured data, the latter is accompanied by a set of data processing routines located in two files. One file is the same as of the measured data and it contains higher level procedures. Whereas, the second one serves as a library of the lower level functions doing the actual 'job'.
- c) To properly assess the accuracy of a model, the LSNA data must be used during the simulations under the same conditions as these of the measurements. Therefore, a link to ADS harmonic balance simulator is established. There are also some external files needed, containing the measurements in a CITI format. This is due to the fact, that IC-CAP has problems working with simulator when the excitation is taken from the IC-CAP output variable.
- d) All these data would be impractical without a graphic user interface straightforward in use. The plot shows the GUI in our case. At the top, it has a set of controls to select the measurements conditions of interest out of the loaded setup. Looking from left to right, the fundamental frequency drop down list, RF power slider and DC bias voltages sliders. Below, there are tabs selecting the domain of the plots displayed at the bottom of the window. User can choose among: V/I or A/B in frequency domain, both VI and AB in time domain, DC drain current, drain output power harmonics, and AM-AM AM-PM in power domain, as well as input, output and transfer locii as dynamic trajectories.



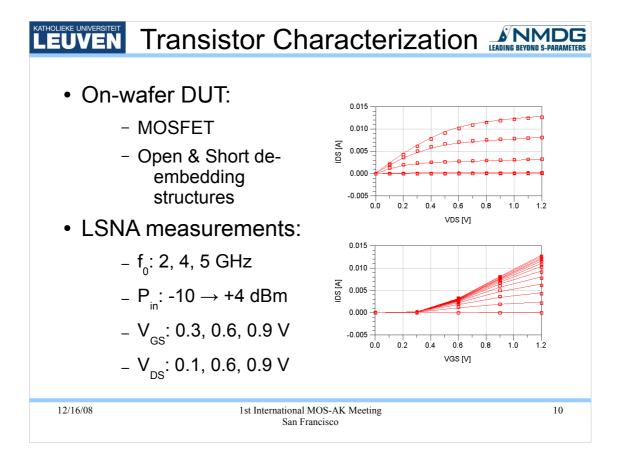
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The described procedure was applied in the characterization of an on-wafer MOSFET device. The DC characteristic of this device are shown on the plots (squares – measurements, lines simulations with Angelov model).

For the de-embedding, we measured open and short dummy structures located on the same wafer and having the same contact pads layout.

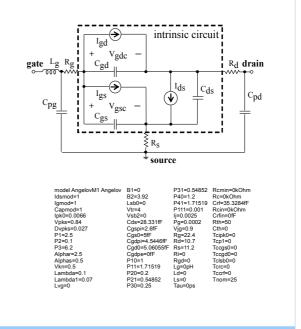
The LSNA measurements were performed on the MOSFET under the reported conditions.



Model verification



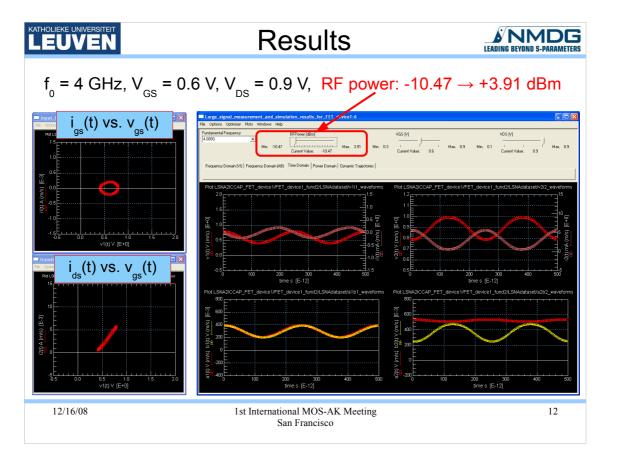
- Angelov MOSFET model:
 - Neglected self-heating and intrinsic non quasi static effects,
 - Capacitance mode,
 - Extracted from DC and S-parameter measurements
 - Tuned around: V_{GS} =0.6 V, V_{DS} =0.9 V, f_{0} =4 GHz

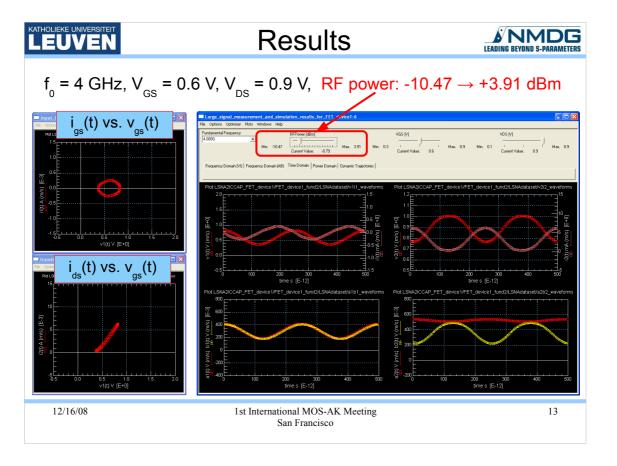


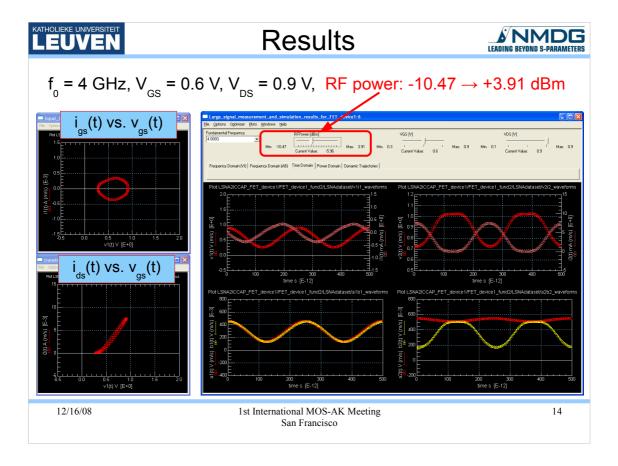
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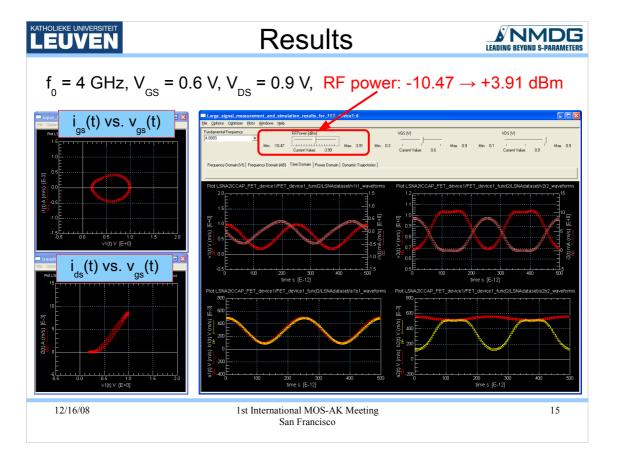
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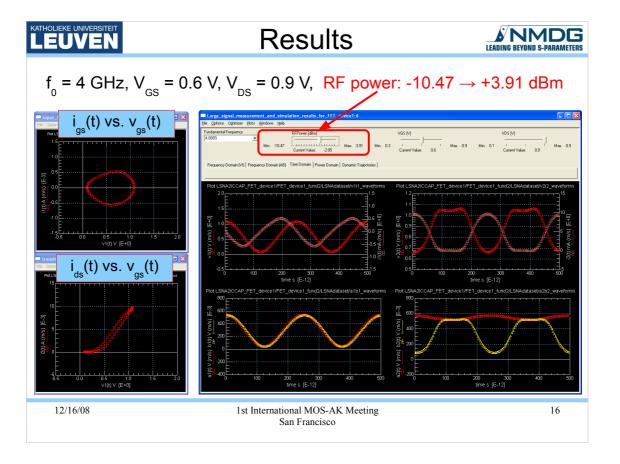
The measurements were applied to verify the accuracy of the Angelov model of the MOSFET device. Due to relatively low operating frequencies the model was simplified as shown on the equivalent circuit plot. The self-heating and intrinsic non quasi static effects were neglected and the capacitance instead of charge mode was used. The model was extracted from previously made DC and S-parameter measurements. The parameters were then tuned around a given bias point and fundamental frequency. The list of the resulting parameters is shown on the slide and it was implemented in IC-CAP.

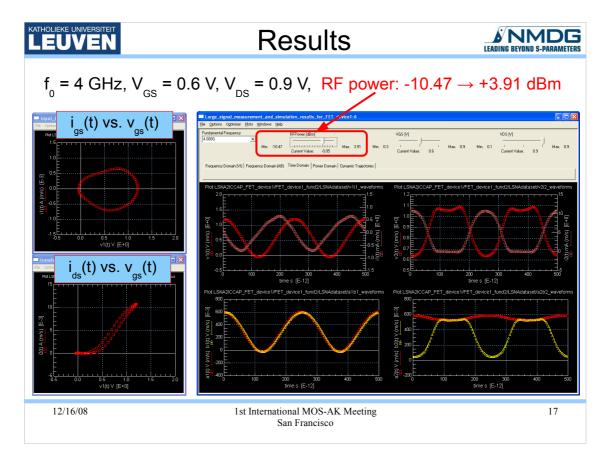


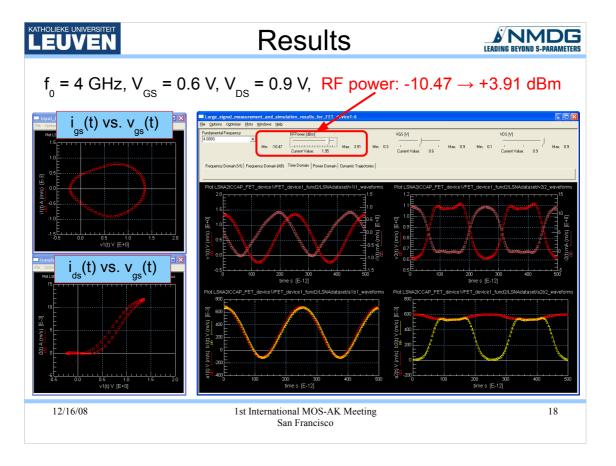


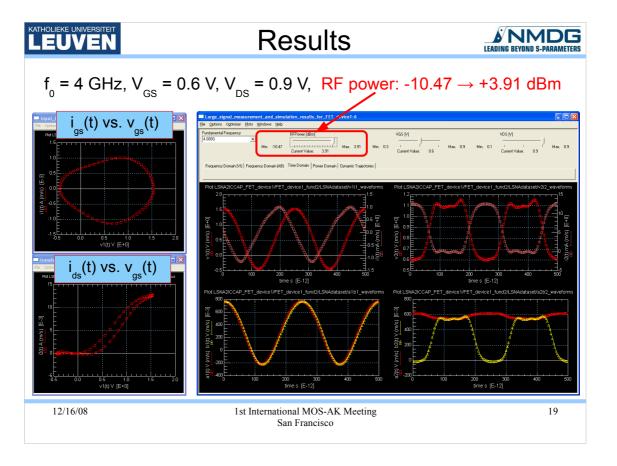


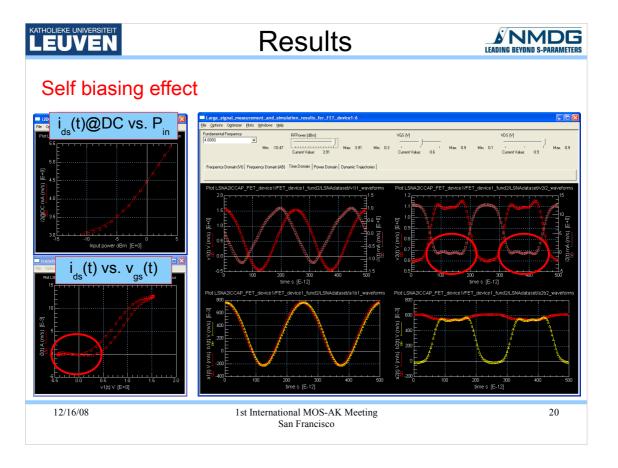




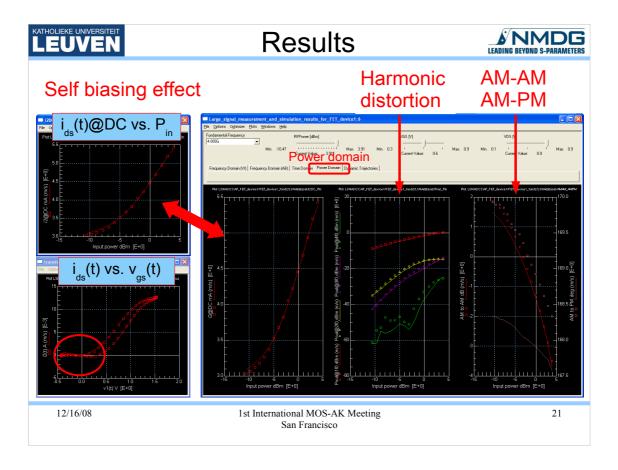




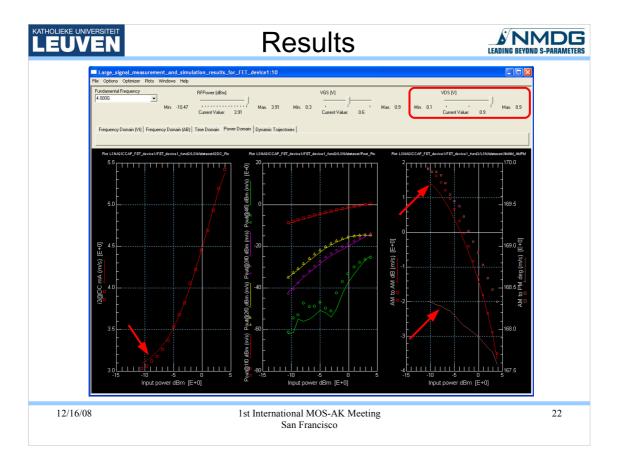




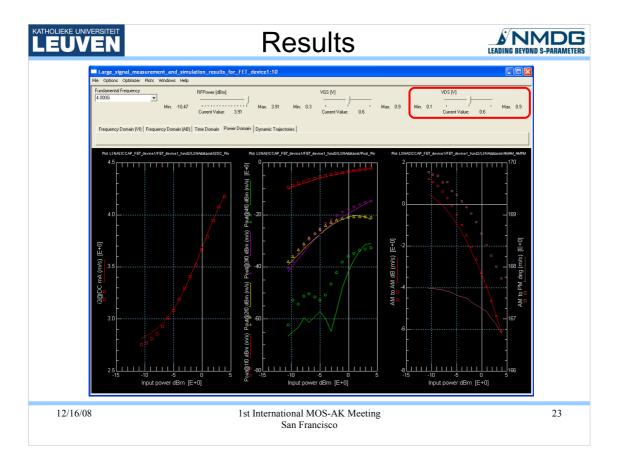
The clipping of the drain current around 0 mA observed both at the time domain and transfer locus plots is related with self biasing effect. This is evident on the next plot, where DC component of the drain current waveform is plotted as function of input power level. The main GUI window also contains this plot under 'Power domain' tab. The other two plots in this set allow observation of harmonic distortion of output signal power, and AM-AM AM-PM characteristics.



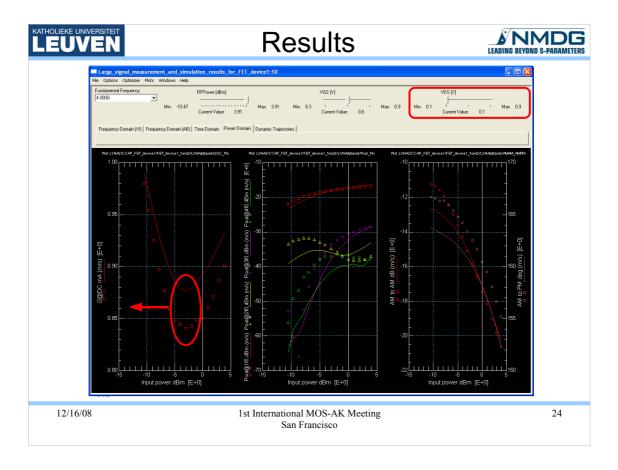
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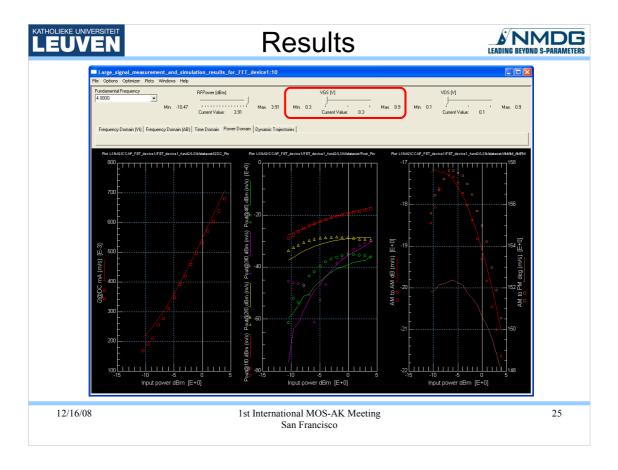
The power domain plots can be also used to test the performance of the model under other DC bias conditions. Therefore, we first sweep the drain DC voltage down to 0.1 V. The overall model's prediction is generally worse than before, but still the match at lower power levels is less accurate. Note that only due to the plot scale, the self biasing seems to be much worse than before.



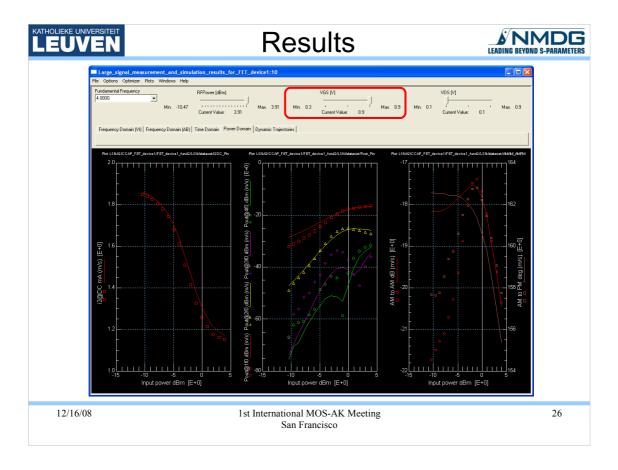
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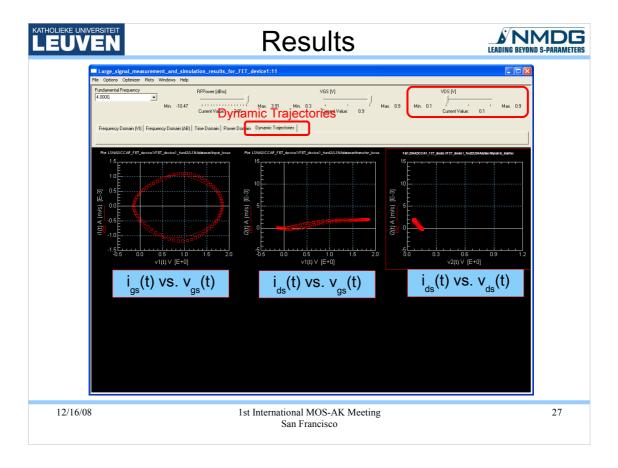
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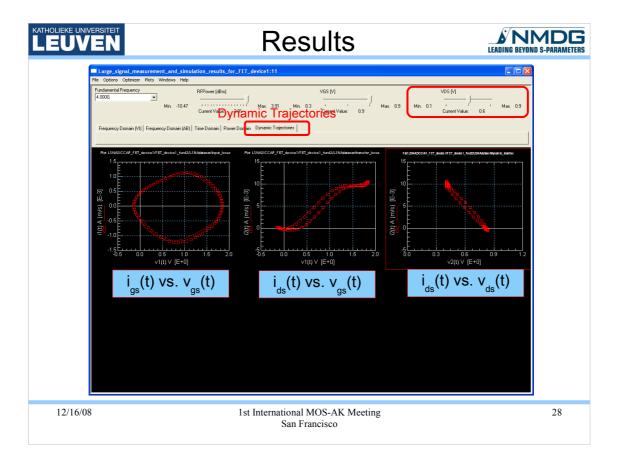
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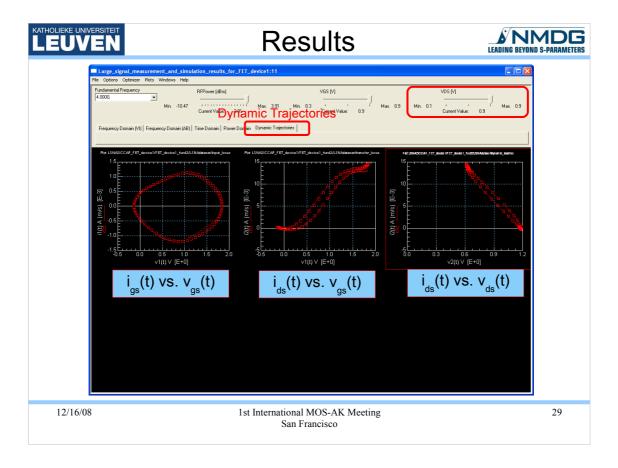
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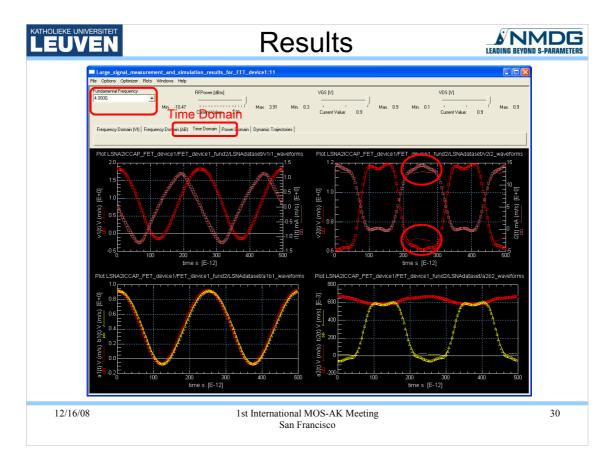
Dynamic trajectories are especially suited for the observation of the drain current behavior under changing DC bias conditions. Look how increasing the drain DC bias voltage changes the transfer and output (dynamic loadline) locii. In both plots we can observe that for a short time the drain current reaches negative values. This is due to a direct coupling through the gate-drain capacitances.

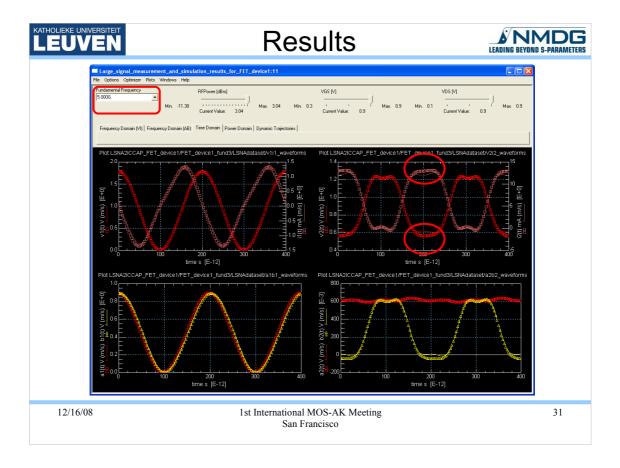


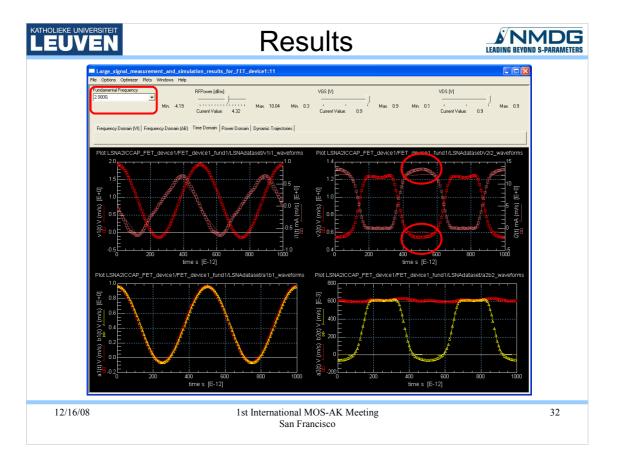
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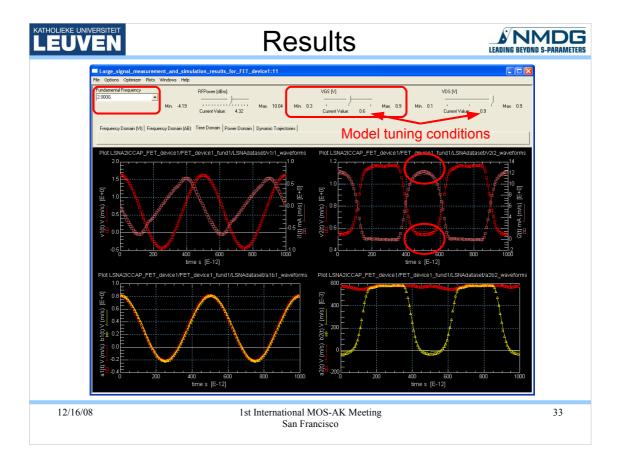


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Conclusions



- Large-signal measurements + device modeling program =
 - Complete large-signal device characterization and model accuracy assessment under realistic signals,
 - Simple access and improved usability of the measured data,
 - Model comparison and optimization.

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