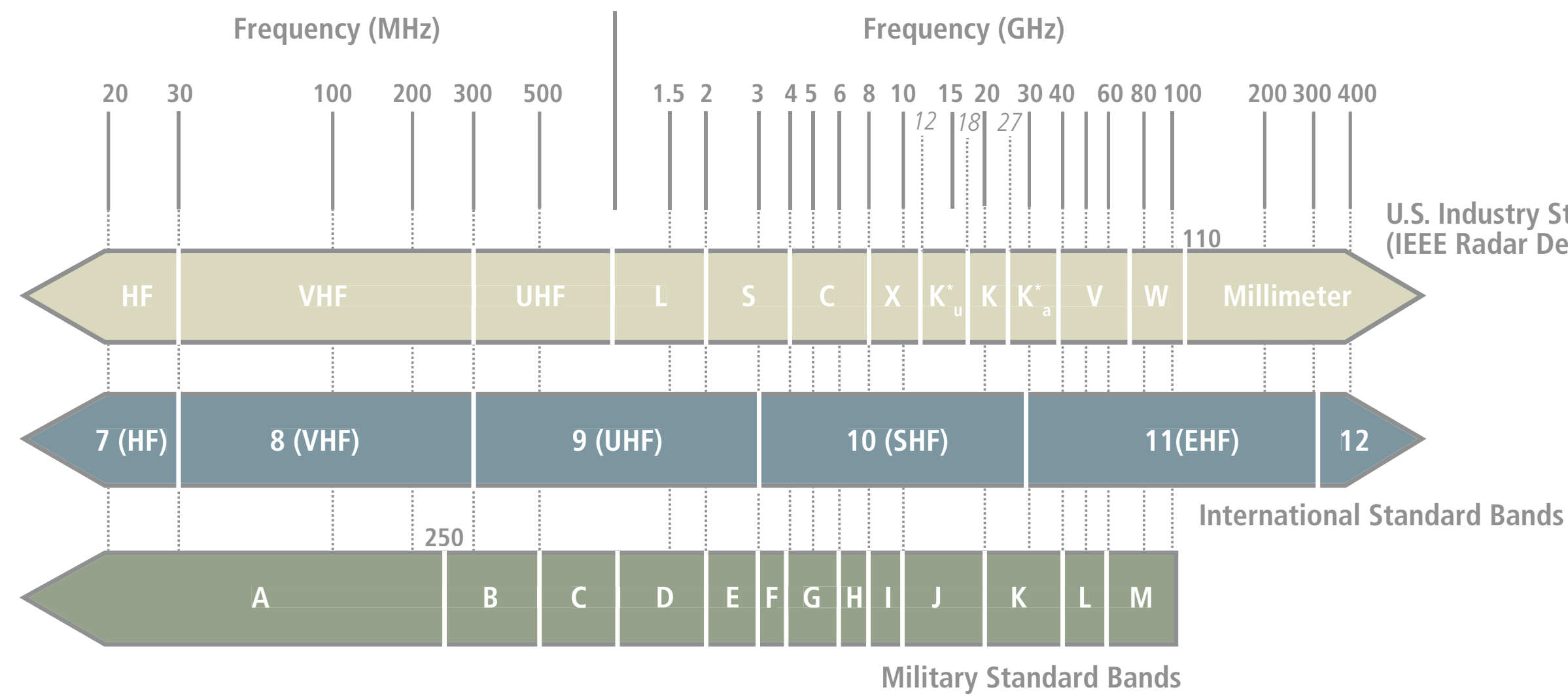
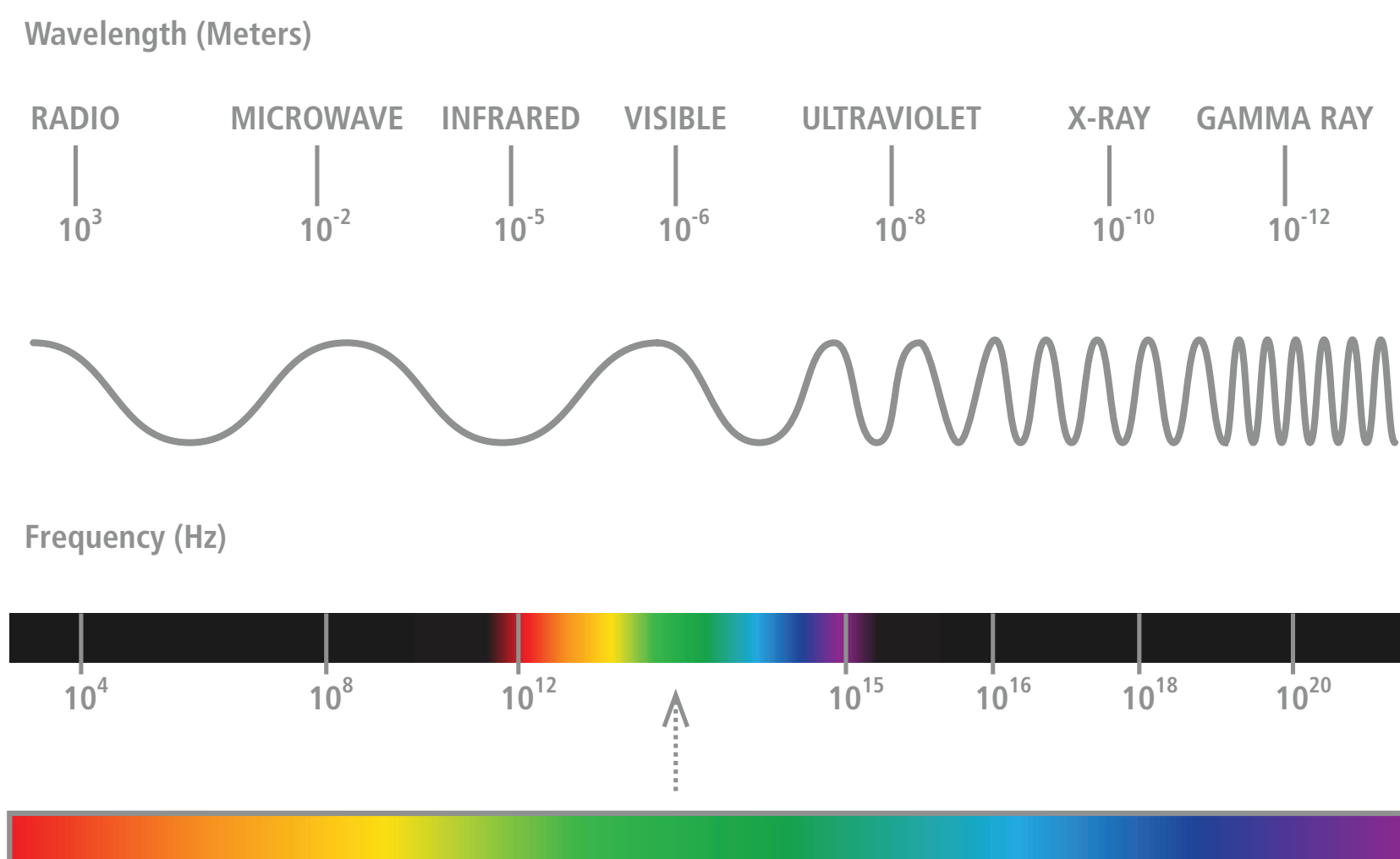


ELECTRONIC WARFARE QUICK REFERENCE GUIDE

THE ELECTROMAGNETIC SPECTRUM



U.S. Industry Standard Bands (IEEE Radar Designation)

Band Designation	Frequency Range
HF	3-30 MHz
VHF	30-300 MHz
UHF	300-1,000 MHz
L	1-2 GHz
S	2-4 GHz
C	4-8 GHz
X	8-12 GHz
K _u	12-18 GHz
K	18-27 GHz
K _a	27-40 GHz
V	40-75 GHz
W	75-110 GHz

* "u" stands for unabsorbed or under K; "a" stands for absorption region or above K

RF Propagation FRIIS TRANSMISSION EQUATION

$$P_r = P_t G_t G_r \left(\frac{\lambda}{4\pi R}\right)^2$$

P_r: Received Power
P_t: Transmit Power
G_t: Transmit Gain
G_r: Receive Gain
R: Range

RF Propagation RADAR HORIZON

$$D_h = \sqrt{2HR_e}$$

H: Horizon
R_e: Earth Radius - 6,371 km

RF Propagation TARGET VISIBILITY

$$\text{Target Height} = \frac{(\text{Target Range} - \sqrt{2HR_e})^2}{2Re}$$

H: Horizon
R_e: Earth Radius - 6,371 km

Detection & Estimation Probability MAX LIKELIHOOD ESTIMATION

Joint Density Function
 $f(x_1, x_2, \dots, x_n | \theta) = f(x_1 | \theta) \times f(x_2 | \theta) \times \dots \times f(x_n | \theta)$

Likelihood
 $L(\theta; x_1, x_2, \dots, x_n) = \prod_{i=1}^n f(x_i | \theta)$

Log-Likelihood
 $\ln L(\theta; x_1, x_2, \dots, x_n) = \sum_{i=1}^n \ln f(x_i | \theta)$

Average Log-Likelihood
 $\hat{\ell} = \frac{1}{n} \ln L$

$\hat{\ell}(\theta|x) = \frac{1}{n} \sum_{i=1}^n \ln f(x_i | \theta)$

Electronic Warfare NOISE JAMMING

$$S = \frac{EIRP_{radar} G_{radar} G_r \lambda^2}{(4\pi)^3 R^4} \sigma$$

$$J/S = \frac{EIRP_{jam} G_{jam} \left(\frac{\lambda}{4\pi R_j}\right)^2 G_{radar}}{EIRP_{radar} \left(\frac{\lambda}{4\pi R_r}\right)^2 G_{radar}}$$

$$J/S = \left(\frac{EIRP_{jam}}{EIRP_{radar}}\right) \left(\frac{4\pi R_r^2}{\sigma}\right) \left(\frac{BW_{radar}}{BW_{jam}}\right)$$

Reduction in Radar Detection Range due to JNR

Reduction in Radar Detection Range due to JNR

Reduction in Normalized Rmax

Normalized Maximum Radar Range vs Jammer to Noise Ratio (dB)

Mainlobe
 $J/N \sim \left(\frac{R_{max}}{R_{max,jammed}}\right)^4$
 Assume: $J \gg N$
 $BW_{jam} = BW_{radar}$

Side-lobe
 $R_{max,jammed} = \frac{P_t G_t' G_r' \lambda^2}{(4\pi)^3 (k T_s B_N N_f + J) * SNR * L_r * L_t}$

Radar Processing LINEAR FM WAVEFORM

$$s(\tau) = e^{i2\pi\left(\tau + \frac{1}{2} b\tau^2\right)}, -\frac{\tau_p}{2} \leq \tau \leq \frac{\tau_p}{2}$$

$$B_p = b\tau_p$$

b: Frequency Chirp Rate
τ_p: Pulse Length
τ: Time Delay
f: Doppler Shift

determines resolution
 determines signal energy

Transmitted Signal Waveform
f_c: Center Frequency
τ: Range Time (fast time)
τ_p: Pulse Length
b: Chirp Rate
B_p: Pulse Bandwidth
f: Range Frequency

Radar Processing RADAR AMBIGUITY FUNCTION

$$x(\tau, t) = \int_{-\infty}^{\infty} s(t) s^*(t-\tau) e^{i2\pi ft} dt$$

S(*t*): Complex Baseband Pulse
τ: Time Delay
f: Doppler Shift

Radar Processing NOISE POWER

$$\text{Noise Power in Receiver} = k T_s B_N N_f$$

k: Boltzmann's constant = 1.38×10^{-23} J/K
T_s: System Noise Temperature
B_N: Noise Bandwidth
N_f: Noise figure of receiver

RF Propagation WAVELENGTH

$$\lambda = \frac{c}{f}$$

Band	f	Wavelength
VHF	100 MHz	3.00 m
S	3 GHz	0.10m
C	6 GHz	0.05m
X	10 GHz	0.03m

c: Speed
f: Frequency

RF Propagation DOPPLER SHIFT

$$f_d = -2v_r / \lambda$$

X-band	S-band
Velocity: 300 m/s	300 m/s
Wavelength: 0.03 m	0.1 m
Doppler Shift: 20 kHz	6 kHz

Detection & Estimation Probability CRAMER RAO LOWER BOUND

$$CRB = \left(E \left[\left[\frac{\partial \ln p(x, \theta)}{\partial \theta} \right] \left[\frac{\partial \ln p(x, \theta)}{\partial \theta} \right]^T \right] \right)^{-1}$$

x: Observations
p: Probability distribution function (or joint)
θ: Distribution parameters can be vectors

Detection & Estimation Probability BINOMIAL

$$f(k; n, p) = \Pr(X=k) = \binom{n}{k} p^k (1-p)^{n-k}$$

p: Success probability of each trial
k: Number of successes
n: Number of trials

Detection & Estimation Probability RAYLEIGH

$$p(r) = \begin{cases} \frac{r}{\sigma^2} e^{-\frac{r^2}{2\sigma^2}} & (r > 0) \\ 0 & (0 \leq r \leq \infty) \end{cases}$$

μ: Mean
σ: Standard Deviation
A: Distance between the reference point and the center of the bivariate distribution

Detection & Estimation Probability ERROR FUNCTIONS

$$\text{erfc}(z) = 1 - \text{erf}(z) = \frac{2}{\sqrt{\pi}} \int_z^{\infty} e^{-t^2} dt$$

$$\text{erf}(z) = \frac{2}{\sqrt{\pi}} \int_0^z e^{-t^2} dt$$

μ: Mean
σ: Standard Deviation
A: Distance between the reference point and the center of the bivariate distribution

Detection & Estimation Probability RICIAN

$$p(r) = \begin{cases} \frac{r}{\sigma^2} e^{-\frac{r^2+A^2}{2\sigma^2}} I_0\left(\frac{Ar}{\sigma^2}\right) & \text{for } (A \geq 0, r \geq 0) \\ 0 & \text{for } (r < 0) \end{cases}$$

μ: Mean
σ: Standard Deviation
A: Distance between the reference point and the center of the bivariate distribution
I₀: Bessel Function of the first kind with order zero

Detection & Estimation Probability NORMAL

$$p(x) = \frac{1}{\sigma\sqrt{2\pi}} e^{-\frac{(x-\mu)^2}{2\sigma^2}}$$

Standard Normal Curve
μ_x = 0; *σ_x* = 1.0

μ: Mean
σ: Standard Deviation
A: Distance between the reference point and the center of the bivariate distribution

Detection & Estimation Probability ERROR FUNCTIONS

$$\text{erfc}(z) = 1 - \text{erf}(z) = \frac{2}{\sqrt{\pi}} \int_z^{\infty} e^{-t^2} dt$$

$$\text{erf}(z) = \frac{2}{\sqrt{\pi}} \int_0^z e^{-t^2} dt$$

μ: Mean
σ: Standard Deviation
A: Distance between the reference point and the center of the bivariate distribution

Fourier Relationships CONTINUOUS-TIME FOURIER TRANSFORMATION

Synthesis
 $x(t) = \int_{-\infty}^{\infty} X(\omega) e^{j\omega t} d\omega$

Analysis
 $X(\omega) = \int_{-\infty}^{\infty} x(t) e^{-j\omega t} dt$

x(*t*) ↔ *X*(*ω*)

Fourier Relationships FILTERING

Ideal Lowpass Filter
 $H(\omega) = \begin{cases} 1 & |\omega| < \omega_c \\ 0 & |\omega| > \omega_c \end{cases}$

Differentiator
 $y(t) = \frac{dx(t)}{dt} \Leftrightarrow H(\omega) = j\omega$

H(*ω*): Frequency Response
⊗: Convolution operation

Fourier Relationships MODULATION PROPERTY

Modulation
 $s(t) p(t) \Leftrightarrow \frac{1}{2\pi} [S(\omega) P(\omega)]$

Convolution
 $h(t) * x(t) \Leftrightarrow H(\omega) X(\omega)$

Time Shifting
 $x(t-t_0) \Leftrightarrow e^{-j\omega t_0} X(\omega)$

Differentiation
 $\frac{dx(t)}{dt} \Leftrightarrow j\omega X(\omega)$

Integration
 $\int_{-\infty}^t x(\tau) d\tau \Leftrightarrow \frac{1}{j\omega} X(\omega) + \pi X(\omega) \delta(\omega)$

Linearity
 $a x_1(t) + b x_2(t) \Leftrightarrow a X_1(\omega) + b X_2(\omega)$

Duality Property

x(*t*) ↔ *X*(*ω*)
X(*ω*) ↔ *x*(*t*)

x(*t*) ↔ *X*(*ω*)
X(*ω*) ↔ *x*(*t*)

x(*t*) ↔ *X*(*ω*)
X(*ω*) ↔ *x*(*t*)

Radar Processing MAX UNAMBIGUOUS RANGE

$$R_{max} = \frac{c}{2PRF}$$

PRF	Range	Doppler	PRF	Unambiguous Range
High	Ambiguous	Unambiguous	100 kHz	1.5 km
Medium	Ambiguous	Ambiguous	25 kHz	6 km
Low	Unambiguous	Ambiguous	10 kHz	15 km

c: Speed of Light
PRF: Pulse Repetition Frequency

Radar Processing SIGNAL TO NOISE RATIO

$$SNR = \frac{P_r}{N_o} = \frac{P_t G_t G_r \sigma \lambda^2 G_p L}{(4\pi)^3 R^4 k T_s B_N N_f}$$

P_r: Received Power
P_t: Transmit Power
G_t: Transmit Gain
G_r: Receive Gain
R: Range
N_o: Noise Power
L: Losses
K: Boltzmann's constant = 1.38×10^{-23} J/K
B_N: Noise Bandwidth
T_s: System Noise Temperature
N_f: Noise figure of receiver

Antennas ANTENNA BEAMWIDTH

Phased Array, Radians
 $\theta_{BW_{3dB}} \sim 0.886 \frac{\lambda}{Nd \cos \theta_0} b$

Parabolic, Radians
 $\theta_{BW_{null}} \sim 1.22 \frac{\lambda}{d}$ $\theta_{BW_{3dB}} \sim 0.88 \frac{\lambda}{d}$

λ: Wavelength
d: Antenna Diameter

Antennas ANTENNA DIRECTIVITY

$$D \approx 4\pi \left(\frac{180}{\pi}\right)^2 \frac{40000}{0.14 \theta_{1d}^2} \approx \frac{40000}{0.14 \theta_{1d}^2}$$

θ_{1d}: Half-power beamwidth in one principal plane (degrees)
θ_{1d}: Half-power beamwidth in the other principal plane (degrees)

Antennas ANTENNA GAIN

$$G_{ant} = \frac{4\pi A_e}{\lambda^2}$$

A_e: Effective Aperture Area
λ: Wavelength

Fourier Relationships CONVOLUTION PROPERTY

$$h(t) * x(t) \Leftrightarrow H(\omega) X(\omega)$$

x(*t*) ↔ *X*(*ω*)
h(*t*) ↔ *H*(*ω*)
h(*t*) * *x*(*t*) ↔ *H*(*ω*) *X*(*ω*)
 $\frac{\delta(t)}{t} \Leftrightarrow \int_{-\infty}^{\infty} \frac{H(\omega)}{j\omega} d\omega$
 $e^{j\omega_c t} \Leftrightarrow H(\omega - \omega_c)$

H(*ω*): Frequency Response
⊗: Convolution operation

Radar Processing RADAR CROSS SECTION

$$\sigma = \frac{\text{Reflected Power to Receiver / Solid Angle}}{\text{Incident Power Density / } 4\pi} = \lim_{r \rightarrow \infty} 4\pi r^2 \left(\frac{|E_s|^2}{|E_i|^2}\right)$$

P_t or *S*
S < *σ*, range
Radar Cross Section (RCS, σ)
 Scattering

Radar Processing TYPICAL VALUES OF RCS

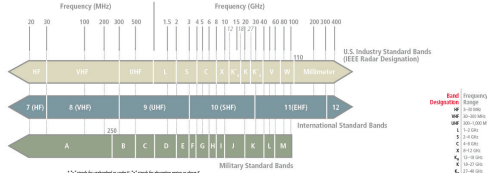
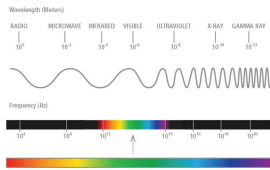
Target	RCS (m²)
Human	~0.01
Small Car	~10
Ship	~1000
Fighter Aircraft	~0.001 - 10
Boeing Stearman Aircraft	~10000

dBsm: -40 to 100

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THE ELECTROMAGNETIC SPECTRUM



<p>Reflection Coefficient</p> $\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}$ <p>Transmission Coefficient</p> $T = \frac{2Z_0}{Z_L + Z_0}$	<p>Return Loss</p> $RL = -20 \log_{10} \Gamma $	<p>Standing Wave Ratio (SWR)</p> $SWR = \frac{1 + \Gamma }{1 - \Gamma }$	<p>Reflection Coefficient (dB)</p> $R_{dB} = 20 \log_{10} \Gamma $	<p>Reflection Coefficient (dB)</p> $R_{dB} = -20 \log_{10} \Gamma $	<p>Reflection Coefficient (dB)</p> $R_{dB} = -20 \log_{10} \Gamma $	<p>Reflection Coefficient (dB)</p> $R_{dB} = -20 \log_{10} \Gamma $	<p>Reflection Coefficient (dB)</p> $R_{dB} = -20 \log_{10} \Gamma $
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