## FEATURES

- 2A Output Current
- Up to 96\% Efficiency
- 4.5 V to 24 V Input Range
- 10ヶA Shutdown Supply Current
- 400kHz Switching Frequency
- Adjustable Output Voltage
- Cycle-by-Cycle Current Limit Protection
- Thermal Shutdown Protection
- Frequency FoldBack at Short Circuit
- Stability with Wide Range of Capacitors, Including Low ESR Ceramic Capacitors
- SOP-8 Package


## APPLICATIONS

- TFT LCD Monitors
- Portable DVDs
- Car-Powered or Battery-Powered Equipments
- Set-Top Boxes
- Telecom Power Supplies
- DSL and Cable Modems and Routers
- Termination Supplies


## GENERAL DESCRIPTION

The ACT4060A is a current-mode step-down DC/DC converter that provides up to 2A of output current at 400 kHz switching frequency. The device utilizes Active-Semi's proprietary high voltage process for operation with input voltages up to 24 V .
The ACT4060A provides fast transient response and eases loop stabilization while providing excellent line and load regulation. This device features a very low ON-resistance power MOSFET which provides peak operating efficiency up to $96 \%$. In shutdown mode, the ACT4060A consumes only $10 \mu \mathrm{~A}$ of supply current.
This device also integrates protection features including cycle-by-cycle current limit, thermal shutdown and frequency fold-back at short circuit.

The ACT4060A is available in a SOP-8 package and requires very few external devices for operation.

## TYPICAL APPLICATION CIRCUIT



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ORDERING INFORMATION

| PART NUMBER | TEMPERATURE RANGE | PACKAGE | PINS | PACKING |
| :---: | :---: | :---: | :---: | :---: |
| ACT4060ASH | $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ | SOP-8 | 8 | TUBE |
| ACT4060ASH-T | $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ | SOP-8 | 8 | TAPE \& REEL |

## PIN CONFIGURATION



## PIN DESCRIPTIONS

| PIN | NAME | DESCRIPTION |
| :---: | :---: | :--- |
| 1 | BS | Bootstrap. This pin acts as the positive rail for the high-side switch's gate driver. <br> Connect a 10nF capacitor between BS and SW. |
| 2 | IN | Input Supply. Bypass this pin to G with a low ESR capacitor. See Input Capacitor <br> in the Application Information section. |
| 3 | SW | Switch Output. Connect this pin to the switching end of the inductor. |
| 4 | G | Ground. |
| 5 | FB | Feedback Input. The voltage at this pin is regulated to 1.293V. Connect to the <br> resistor divider between output and ground to set output voltage. |
| 6 | COMP | Compensation Pin. See Stability Compensation in the Application Information <br> section. |
| 7 | N/C | Enable Input. When higher than 1.3V, this pin turns the IC on. When lower than <br> 0.7 V, this pin turns the IC off. Output voltage is discharged when the IC is off. <br> When left unconnected, EN is pulled up to 4.5V with a 2 2 AA pull-up current. |
| 8 | Not Connected. |  |

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## ABSOLUTE MAXIMUM RATINGS ${ }^{\oplus}$

| PARAMETER | VALUE | UNIT |
| :--- | :---: | :---: |
| IN Supply Voltage | -0.3 to 28 | V |
| SW Voltage | -1 to $\mathrm{V}_{\text {IN }}+1$ | V |
| BS Voltage | $\mathrm{V}_{\text {Sw }}-0.3$ to $\mathrm{V}_{\text {SW }}+8$ | V |
| EN, FB, COMP Voltage | -0.3 to 6 | V |
| Continuous SW Current | Internally Limited | A |
| Junction to Ambient Thermal Resistance $\left(\theta_{\mathrm{JA}}\right)$ | 105 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| Maximum Power Dissipation | 0.76 | W |
| Operating Junction Temperature | -40 to 150 | ${ }^{\circ} \mathrm{C}$ |
| Storage Temperature | -55 to 150 | ${ }^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 10 sec ) | 300 | ${ }^{\circ} \mathrm{C}$ |

(1): Do not exceed these limits to prevent damage to the device. Exposure to absolute maximum rating conditions for long periods may affect device reliability.

## ELECTRICAL CHARACTERISTICS

$\left(\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}\right.$, unless otherwise specified.)

| PARAMETER | SYMBOL | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input Voltage | $\mathrm{V}_{\text {IN }}$ | $\mathrm{V}_{\text {OUT }}=3.3 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=0 \mathrm{~A}$ to 1 A | 4.5 |  | 24 | V |
| Feedback Voltage | $V_{\text {FB }}$ | $4.5 \mathrm{~V} \leq \mathrm{V}_{\text {IN }} \leq 24 \mathrm{~V}, \mathrm{~V}_{\text {COMP }}=1.5 \mathrm{~V}$ | 1.267 | 1.293 | 1.319 | V |
| High-Side Switch On Resistance | $\mathrm{R}_{\text {ONH }}$ |  |  | 0.18 |  | $\Omega$ |
| Low-Side Switch On Resistance | RonL |  |  | 4.5 |  | $\Omega$ |
| SW Leakage |  | $\mathrm{V}_{\mathrm{EN}}=0$ |  | 0 | 10 | $\mu \mathrm{A}$ |
| Current Limit | $\mathrm{I}_{\text {LIM }}$ |  | 2.4 | 2.85 |  | A |
| COMP to Current Limit Transconductance | $\mathrm{G}_{\text {comp }}$ | $\mathrm{V}_{\text {IN }}=12 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=5 \mathrm{~V}$ |  | 1.8 |  | A/V |
| Error Amplifier Transconductance | $\mathrm{G}_{\text {EA }}$ | $\Delta \mathrm{I}_{\text {COMP }}= \pm 10 \mu \mathrm{~A}$ |  | 650 |  | $\mu \mathrm{A} / \mathrm{V}$ |
| Error Amplifier DC Gain | $A_{\text {VEA }}$ |  |  | 4000 |  | V/V |
| Switching Frequency | $\mathrm{f}_{\mathrm{sw}}$ |  | 350 | 400 | 450 | kHz |
| Short Circuit Switching Frequency |  | $\mathrm{V}_{\mathrm{FB}}=0$ |  | 60 |  | kHz |
| Maximum Duty Cycle | $\mathrm{D}_{\text {MAX }}$ | $\mathrm{V}_{\mathrm{FB}}=1.1 \mathrm{~V}$ |  | 95 |  | \% |
| Minimum Duty Cycle |  | $\mathrm{V}_{\mathrm{FB}}=1.4 \mathrm{~V}$ |  |  | 0 | \% |
| Enable Threshold Voltage |  | Hysteresis $=0.1 \mathrm{~V}$ | 0.7 | 1 | 1.3 | V |
| Enable Pull-Up Current |  | Pin pulled up to 4.5 V typically when left unconnected |  | 2 |  | $\mu \mathrm{A}$ |
| Supply Current in Shutdown |  | $\mathrm{V}_{\mathrm{EN}}=0$ |  | 10 | 20 | $\mu \mathrm{A}$ |
| IC Supply Current in Operation |  | $\mathrm{V}_{\mathrm{EN}}=3 \mathrm{~V}, \mathrm{~V}_{\mathrm{FB}}=1.4 \mathrm{~V}$ |  | 0.55 |  | mA |
| Thermal Shutdown Temperature |  | Hysteresis $=10^{\circ} \mathrm{C}$ |  | 160 |  | ${ }^{\circ} \mathrm{C}$ |

## FUNCTIONAL BLOCK DIAGRAM



## FUNCTIONAL DESCRIPTION

As seen in Functional Block Diagram, the ACT4060A is a current mode pulse width modulation (PWM) converter. The converter operates as follows:

A switching cycle starts when the rising edge of the Oscillator clock output causes the High-Side Power Switch to turn on and the Low-Side Power Switch to turn off. With the SW side of the inductor now connected to IN, the inductor current ramps up to store energy in the magnetic field. The inductor current level is measured by the Current Sense Amplifier and added to the Oscillator ramp signal. If the resulting summation is higher than the COMP voltage, the output of the PWM Comparator goes high. When this happens or when Oscillator clock output goes low, the High-Side Power Switch turns off and the Low-Side Power Switch turns on. At this point, the SW side of the inductor swings to a diode voltage below ground, causing the inductor current to decrease and magnetic energy to be transferred to output. This state continues until the cycle starts again.

The High-Side Power Switch is driven by logic using BS as the positive rail. This pin is charged to $\mathrm{V}_{\mathrm{sw}}+$ 6 V when the Low-Side Power Switch turns on.

The COMP voltage is the integration of the error between FB input and the internal 1.293 V
reference. If FB is lower than the reference voltage, COMP tends to go higher to increase current to the output. Current limit happens when COMP reaches its maximum clamp value of 2.55 V .
The Oscillator normally switches at 400 kHz . However, if FB voltage is less than 0.7 V , then the switching frequency decreases until it reaches a typical value of 60 kHz at $\mathrm{V}_{\mathrm{FB}}=0.5 \mathrm{~V}$.

## Shutdown Control

The ACT4060A has an enable input EN for turning the IC on or off. When EN is less than 0.7 V , the IC is in $10 \mu \mathrm{~A}$ low current shutdown mode and output is discharged through the Low-Side Power Switch. When EN is higher than 1.3 V , the IC is in normal operation mode. EN is internally pulled up with a $2 \mu \mathrm{~A}$ current source and can be left unconnected for always-on operation. Note that EN is a low voltage input with a maximum voltage of 6 V , it should never be directly connected to IN.

## Thermal Shutdown

The ACT4060A automatically turns off when its junction temperature exceeds $160^{\circ} \mathrm{C}$.

## APPLICATIONS INFORMATION

## Output Voltage Setting

Figure 1:

## Output Voltage Setting



Figure 1 shows the connections for setting the output voltage. Select the proper ratio of the two feedback resistors $R_{F B 1}$ and $R_{\text {FB2 }}$ based on the output voltage. Typically, use $R_{F B 2} \approx 10 \mathrm{k} \Omega$ and determine $R_{\text {FB1 }}$ from the following equation:
$R_{F B 1}=R_{\text {FB2 }}\left(\frac{V_{\text {OUT }}}{1.293 V}-1\right)$

## Inductor Selection

The inductor maintains a continuous current to the output load. This inductor current has a ripple that is dependent on the inductance value: higher inductance reduces the peak-to-peak ripple current. The trade off for high inductance value is the increase in inductor core size and series resistance, and the reduction in current handling capability. In general, select an inductance value $L$ based on ripple current requirement:
$L=\frac{V_{\text {OUT }} \times\left(V_{\text {IN }}-V_{\text {OUT }}\right)}{V_{\text {IN }} f_{\text {SW }} I_{\text {OUTMAX }} K_{\text {RIPPLE }}}$
where $\mathrm{V}_{\mathbb{I N}}$ is the input voltage, $\mathrm{V}_{\text {OUt }}$ is the output voltage, $\mathrm{f}_{\mathrm{Sw}}$ is the switching frequency, loutmax is the maximum output current, and $\mathrm{K}_{\text {RIPPLE }}$ is the ripple factor. Typically, choose $\mathrm{K}_{\text {RIPPLE }}=30 \%$ to correspond to the peak-to-peak ripple current being $30 \%$ of the maximum output current.

With this inductor value, the peak inductor current is lout $\times\left(1+\mathrm{K}_{\text {RIPPLE }} / 2\right)$. Make sure that this peak inductor current is less that the 3A current limit. Finally, select the inductor core size so that it does not saturate at 3A. Typical inductor values for various output voltages are shown in Table 1.

Table 1:
Typical Inductor Values

| V Out | $\mathbf{1 . 5 V}$ | $\mathbf{1 . 8 V}$ | $\mathbf{2 . 5 V}$ | $\mathbf{3 . 3 V}$ | $\mathbf{5 V}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L | $6.8 \mu \mathrm{H}$ | $6.8 \mu \mathrm{H}$ | $10 \mu \mathrm{H}$ | $15 \mu \mathrm{H}$ | $22 \mu \mathrm{H}$ |

## Input Capacitor

The input capacitor needs to be carefully selected to maintain sufficiently low ripple at the supply input of the converter. A low ESR capacitor is highly recommended. Since large current flows in and out of this capacitor during switching, its ESR also affects efficiency

The input capacitance needs to be higher than $10 \mu \mathrm{~F}$. The best choice is the ceramic type, however, low ESR tantalum or electrolytic types may also be used provided that the RMS ripple current rating is higher than $50 \%$ of the output current. The input capacitor should be placed close to the $I N$ and $G$ pins of the $I C$, with the shortest traces possible. In the case of tantalum or electrolytic types, they can be further away if a small parallel $0.1 \mu \mathrm{~F}$ ceramic capacitor is placed right next to the IC.

## Output Capacitor

The output capacitor also needs to have low ESR to keep low output voltage ripple. The output ripple voltage is:
$V_{\text {RIPPLE }}=I_{\text {OUTMAX }} K_{\text {RIPPLE }} R_{\text {ESR }}$
$+\frac{V_{\text {IN }}}{28 \times f_{\text {SW }}{ }^{2} L C_{\text {OUT }}}$
where loutmax is the maximum output current, $\mathrm{K}_{\text {RIPPLE }}$ is the ripple factor, $\mathrm{R}_{\text {ESR }}$ is the ESR of the output capacitor, $f_{S W}$ is the switching frequency, $L$ is the inductor value, and $\mathrm{C}_{\text {out }}$ is the output capacitance. In the case of ceramic output capacitors, $R_{\text {ESR }}$ is very small and does not contribute to the ripple. Therefore, a lower capacitance value can be used for ceramic type. In the case of tantalum or electrolytic capacitors, the ripple is dominated by $\mathrm{R}_{\text {ESR }}$ multiplied by the ripple current. In that case, the output capacitor is chosen to have sufficiently low ESR.

For ceramic output capacitor, typically choose a capacitance of about $22 \mu \mathrm{~F}$. For tantalum or electrolytic capacitors, choose a capacitor with less than $50 \mathrm{~m} \Omega \mathrm{ESR}$.

## Rectifier Diode

Use a Schottky diode as the rectifier to conduct current when the High-Side Power Switch is off. The Schottky diode must have current rating higher than the maximum output current and a reverse voltage rating higher than the maximum input voltage.

## STABILITY COMPENSATION

Figure 2:

## Stability Compensation


(1): $\mathrm{C}_{\text {comp2 }}$ is needed only for high ESR output capacitor

The feedback loop of the IC is stabilized by the components at the COMP pin, as shown in Figure 2. The DC loop gain of the system is determined by the following equation:
$A_{V D C}=\frac{1.3 V}{I_{\text {OUT }}} A_{V E A} G_{\text {COMP }}$
The dominant pole P 1 is due to $\mathrm{C}_{\text {сомр }}$ :
$f_{P 1}=\frac{G_{E A}}{2 \pi A_{V E A} C_{\text {COMr }}}$
The second pole P2 is the output pole:
$f_{P 2}=\frac{I_{\text {OUT }}}{2 \pi V_{\text {OUT }} C_{\text {OUT }}}$
The first zero Z 1 is due to $\mathrm{R}_{\text {сомр }}$ and $\mathrm{C}_{\text {сомр }}$ :
$f_{Z 1}=\frac{1}{2 \pi R_{\text {СОМР }} C_{\text {Сом }}}$
And finally, the third pole is due to $R_{\text {COMP }}$ and $\mathrm{C}_{\text {COMP2 }}$ (if $\mathrm{C}_{\text {COMP2 }}$ is used):
$f_{P 3}=\frac{1}{2 \pi R_{\text {COMP }} C_{\text {COMP2 }}}$
The following steps should be used to compensate the IC:

STEP 1. Set the cross over frequency at $1 / 10$ of the switching frequency via $\mathrm{R}_{\text {сомр }}$ :

$$
\begin{align*}
& R_{\text {COMP }}=\frac{2 \pi V_{\text {OUT }} C_{\text {OUT }} f_{S W}}{10 G_{\text {EA }} G_{\text {COMP }} \times 1.3 V} \\
& =1.7 \times 10^{8} V_{\text {OUT }} C_{\text {OUT }}
\end{align*}
$$

STEP 2. Set the zero $f_{Z 1}$ at $1 / 4$ of the cross over frequency. If $R_{\text {Comp }}$ is less than $15 k \Omega$, the equation for $\mathrm{C}_{\text {сомр }}$ is:
$C_{\text {COMP }}=\frac{1.8 \times 10^{-5}}{R_{\text {COMP }}}$
If $R_{\text {Comp }}$ is limited to $15 \mathrm{k} \Omega$, then the actual cross over frequency is 3.4 / ( $\left.\mathrm{V}_{\text {OUT }} \mathrm{C}_{\text {OUT }}\right)$. Therefore:
$C_{\text {COMP }}=1.2 \times 10^{-5} V_{\text {OUT }} C_{\text {OUT }}$
STEP 3. If the output capacitor's ESR is high enough to cause a zero at lower than 4 times the cross over frequency, an additional compensation capacitor $\mathrm{C}_{\text {COMP2 }}$ is required. The condition for using $\mathrm{C}_{\text {Comp2 }}$ is:
$R_{\text {ESRCOUT }} \geq \operatorname{Min}\left(\frac{1.1 \times 10^{-6}}{C_{\text {OUT }}}, 0.012 \times V_{\text {OUT }}\right)$
And the proper value for $\mathrm{C}_{\text {COMP2 }}$ is:
$C_{\text {COMP2 }}=\frac{C_{\text {OUT }} R_{\text {ESRCOUT }}}{R_{\text {COMP }}}$
Though $\mathrm{C}_{\text {Comp2 }}$ is unnecessary when the output capacitor has sufficiently low ESR, a small value $\mathrm{C}_{\text {Comp2 }}$ such as 100 pF may improve stability against PCB layout parasitic effects.

Table 2 shows some calculated results based on the compensation method above.

Table 2:
Typical Compensation for Different Output Voltages and Output Capacitors

| $\mathrm{V}_{\text {OUT }}$ | C $_{\text {out }}$ | $\mathbf{R}_{\text {Comp }}$ | $\mathbf{C}_{\text {comp }}$ |
| :---: | :---: | :---: | :---: |
| 2.5 V | $22 \mu \mathrm{~F}$ Ceramic | $8.2 \mathrm{k} \Omega$ | 2.2 nF |
| 3.3 V | $22 \mu \mathrm{~F}$ Ceramic | $12 \mathrm{k} \Omega$ | 1.5 nF |
| 5 V | $22 \mu \mathrm{~F}$ Ceramic | $15 \mathrm{k} \Omega$ | 1.5 nF |
| 2.5 V | $47 \mu \mathrm{~F} \mathrm{SP} \mathrm{CAP}$ | $15 \mathrm{k} \Omega$ | 1.5 nF |
| 3.3 V | $47 \mu \mathrm{~F} \mathrm{SP} \mathrm{CAP}$ | $15 \mathrm{k} \Omega$ | 1.8 nF |
| 5 V | $47 \mu \mathrm{~F} \mathrm{SP} \mathrm{CAP}$ | $15 \mathrm{k} \Omega$ | 2.7 nF |
| 2.5 V | $470 \mu \mathrm{~F} / 6.3 \mathrm{~V} / 30 \mathrm{~m} \Omega$ | $15 \mathrm{k} \Omega$ | 15 nF |
| 3.3 V | $470 \mu \mathrm{~F} / 6.3 \mathrm{~V} / 30 \mathrm{~m} \Omega$ | $15 \mathrm{k} \Omega$ | 22 nF |
| 5 V | $470 \mu \mathrm{~F} / 6.3 \mathrm{~V} / 30 \mathrm{~m} \Omega$ | $15 \mathrm{k} \Omega$ | 27 nF |

Figure 4 shows an example ACT4060A application circuit generating a $3.3 \mathrm{~V} / 2 \mathrm{~A}$ output.

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## ACT4060A PCB Layout Guidelines.

Place all the power components (Diode, Inductor, filter Capacitors) as close as possible. Use short and wide trace between them.

If double layer PCB is used, it is good if the bottom layer is almost fill as ground. Use ground planes for power ground and signal ground, connect signal ground and power ground at single point close to the IC GND.

Arrange the power components so that the switching current loop curl in the same direction.

Separate noise sensitive traces, such as the voltage feedback path, compensation from noisy sources such as inductor, diode, input capacitor.

Place components, such as compensation, feedback network and boost-trap capacitors, as close to the IC as possible.

Ceramic cap C 1 is closely placed across $\mathrm{V}_{\mathbb{I N}}$ and GND of the IC, as close as possible.

Figure 3:

## ACT4060A PCB Layout Reference



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Figure 4:

## ACT4060A 3.3V/2A Output Application ${ }^{\text {® }}$


(1): D1 is a 40V, 3A Schottky diode with low forward voltage, an IR 30BQ040 or SK34 equivalent. C4 can be either a ceramic capacitor (Panasonic ECJ-3YB1C226M) or SP-CAP (Specialty Polymer) Aluminum Electrolytic Capacitor such as Panasonic EEFCD0J470XR. The SP-Cap is based on aluminum electrolytic capacitor technology, but uses a solid polymer electrolyte and has very stable capacitance characteristics in both operating temperature and frequency compared to ceramic, polymer, and low ESR tantalum capacitors.

Table 3:
ACT4060A Bill of Materials (Apply for 3.3V Output Application)

| ITEM | DESCRIPTION | MANUFACTURER | QTY | REFERENCE |
| :---: | :---: | :---: | :---: | :---: |
| 1 | IC, ACT4060A | Active-Semi | 1 | U1 |
| 2 | $15 \mu \mathrm{H} \pm 20 \%, \mathrm{I}_{\text {SAT }}=2.7 \mathrm{~A}, \mathrm{I}_{\mathrm{DC}}=2.4 \mathrm{~A} @ \Delta \mathrm{~T}=40^{\circ} \mathrm{C}$ | Taiyo Yuden NR 8040T 150M | 1 | L1 |
|  | $15 \mu \mathrm{H} \pm 10 \%, \mathrm{I}_{\text {SAT }}=2.88 \mathrm{~A}, \mathrm{I}_{\mathrm{DC}}=2.47 \mathrm{~A} @ \Delta \mathrm{~T}=40^{\circ} \mathrm{C}$ | Wurth Electronik 744776115 |  |  |
|  | $10 \mu \mathrm{H} \pm 20 \%, \mathrm{I}_{\text {SAT }}=3.4 \mathrm{~A}, \mathrm{I}_{\mathrm{DC}}=2.5 \mathrm{~A} @ \Delta \mathrm{~T}=40^{\circ} \mathrm{C}$ | Taiyo Yuden NR 6045T 100M |  |  |
|  | $10 \mu \mathrm{H} \pm 10 \%, \mathrm{I}_{\text {SAT }}=2.95 \mathrm{~A}, \mathrm{I}_{\mathrm{DC}}=2.3 \mathrm{~A} @ \Delta \mathrm{~T}=40^{\circ} \mathrm{C}$ | Wurth Electronik 74477510 |  |  |
| 3 | Schottky Diode SK34/40V, 3A, SMB | Transys electronics | 1 | D1 |
|  | Schottky Diode B340C/40V, 3A, SMB | Diodes Inc | 1 |  |
| 4 | Ceramic cap $10 \mu \mathrm{~F} / 35 \mathrm{~V}, \mathrm{X} 7 \mathrm{R}, 1210$ | Murata, TDK, Taiyo Yuden | 1 | C1 |
| 5 | Ceramic cap 2.2nF/6.3V, X7R, 0603 | Murata, TDK, Taiyo Yuden | 1 | C2 |
| 6 | Ceramic cap 10nF/50V, X7R, 0603 | Murata, TDK, Taiyo Yuden | 1 | C3 |
| 7 | Ceramic cap $22 \mu \mathrm{~F} / 10 \mathrm{~V}, \mathrm{X} 7 \mathrm{R}, 1210$ | Murata, TDK,Taiyo Yuden | 1 | C4 |
|  | SP cap $47 \mu \mathrm{~F} / 6.3 \mathrm{~V}, 50 \mathrm{~m} \Omega$ | Kemet, Panasonic |  |  |
| 8 | Resistor, 15.5k , 1/16W, 1\%, 0603 | FengHua, Neohm, Yageo | 1 | R1 |
| 9 | Resistor, 10k ${ }^{\text {, 1/16W, 1\%, } 0603}$ |  |  | R2 |
| 10 | Resistor, 12k , 1/16W, 5\%, 0603 |  |  | R3 |

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Figure 5:

## ACT4060A 5V/2A Output Application ${ }^{\circledR}$


(1): D1 is a 40V, 3A Schottky diode with low forward voltage, an IR 30BQ040 or SK34 equivalent. C4 can be either a ceramic capacitor (Panasonic ECJ-3YB1C226M) or SP-CAP (Specialty Polymer) Aluminum Electrolytic Capacitor such as Panasonic EEFCD0J470XR. The SP-Cap is based on aluminum electrolytic capacitor technology, but uses a solid polymer electrolyte and has very stable capacitance characteristics in both operating temperature and frequency compared to ceramic, polymer, and low ESR tantalum capacitors.

Table 4:
ACT4060A Bill of Materials (Apply for 5V Output Application)

| ITEM | DESCRIPTION | MANUFACTURER | QTY | REFERENCE |
| :---: | :---: | :---: | :---: | :---: |
| 1 | IC, ACT4060A | Active-Semi | 1 | U1 |
| 2 | $15 \mu \mathrm{H} \pm 20 \%, \mathrm{I}_{\text {SAT }}=2.7 \mathrm{~A}, \mathrm{I}_{\mathrm{DC}}=2.4 \mathrm{~A} @ \Delta \mathrm{~T}=40^{\circ} \mathrm{C}$ | Taiyo Yuden NR 8040T 150M | 1 | L1 |
|  | $15 \mu \mathrm{H} \pm 10 \%, \mathrm{I}_{\text {SAT }}=2.88 \mathrm{~A}, \mathrm{I}_{\mathrm{DC}}=2.47 \mathrm{~A} @ \Delta \mathrm{~T}=40^{\circ} \mathrm{C}$ | Wurth Electronik 744776115 |  |  |
| 3 | Schottky Diode SK34/40V, 3A, SMB | Transys electronics | 1 | D1 |
|  | Schottky Diode B340C/40V, 3A, SMB | Diodes Inc |  |  |
| 4 | Ceramic cap 10رF/35V, X7R, 1210 | Murata, TDK, Taiyo Yuden | 1 | C1 |
| 5 | Ceramic cap 2.2nF/6.3V, X7R, 0603 | Murata, TDK, Taiyo Yuden | 1 | C2 |
| 6 | Ceramic cap 10nF/50V, X7R, 0603 | Murata, TDK, Taiyo Yuden | 1 | C3 |
| 7 | Ceramic cap $22 \mu \mathrm{~F} / 10 \mathrm{~V}$, X7R, 1210 | Murata, TDK, Taiyo Yuden | 1 | C4 |
|  | SP cap $47 \mu \mathrm{~F} / 6.3 \mathrm{~V}, 50 \mathrm{~m} \Omega$ | Kemet, Panasonic |  |  |
| 8 | Resistor, 28.7k $\Omega$, 1/16W, 1\%, 0603 | FengHua, Neohm, Yageo | 1 | R1 |
| 9 | Resistor, 10k ${ }^{\text {, 1/16W, 1\%, } 0603}$ |  |  | R2 |
| 10 | Resistor, 15k ${ }^{\text {, 1/16W, 5\%, } 0603}$ |  |  | R3 |

## TYPICAL PERFORMANCE CHARACTERISTICS

(Circuit of Figure 4, unless otherwise specified.)


Efficiency vs. Output Current


Switching Frequency vs. Input Voltage


Efficiency vs. Output Current


Maximum Output Current vs. Duty Cycle


Feedback Voltage vs. Temperature


## TYPICAL PERFORMANCE CHARACTERISTICS CONT'D

(Circuit of Figure 4, unless otherwise specified.)


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## PACKAGE OUTLINE

## SOP-8 PACKAGE OUTLINE AND DIMENSIONS



Active-Semi, Inc. reserves the right to modify the circuitry or specifications without notice. Users should evaluate each product to make sure that it is suitable for their applications. Active-Semi products are not intended or authorized for use as critical components in life-support devices or systems. Active-Semi, Inc. does not assume any liability arising out of the use of any product or circuit described in this datasheet, nor does it convey any patent license.

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