

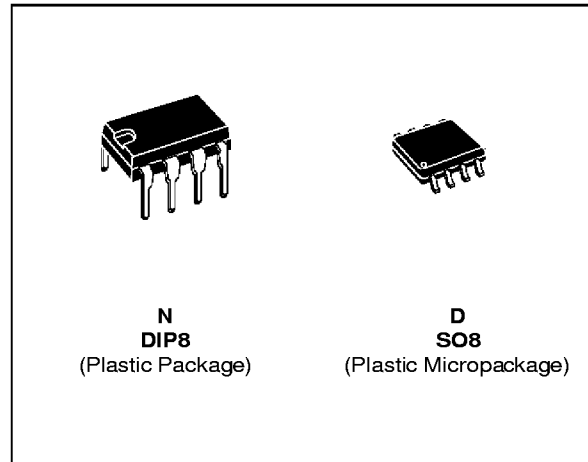
## HIGH PERFORMANCE DUAL OPERATIONAL AMPLIFIERS

- LOW POWER CONSUMPTION
- SHORT CIRCUIT PROTECTION
- LOW DISTORTION, LOW NOISE
- HIGH GAIN-BANDWIDTH PRODUCT
- HIGH CHANNEL SEPARATION

### DESCRIPTION

The LS204 is a high performance dual operational amplifier with frequency and phase compensation built into the chip. The internal phase compensation allows stable operation as voltage follower in spite of its high gain-bandwidth products.

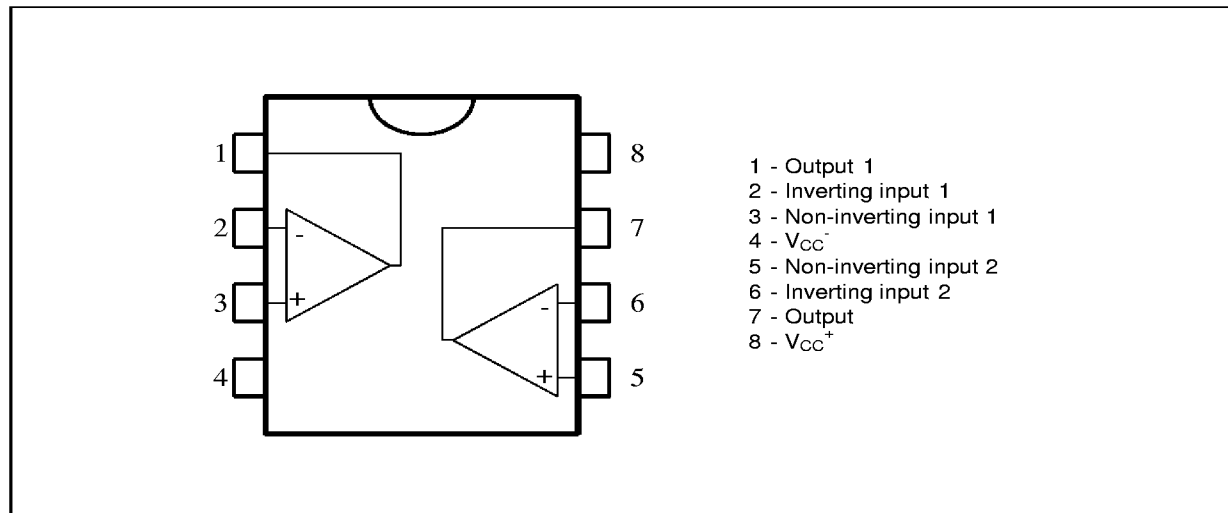
The circuit presents very stable electrical characteristics over the entire supply voltage range, and is particularly intended for professional and telecom applications (active filters, etc).



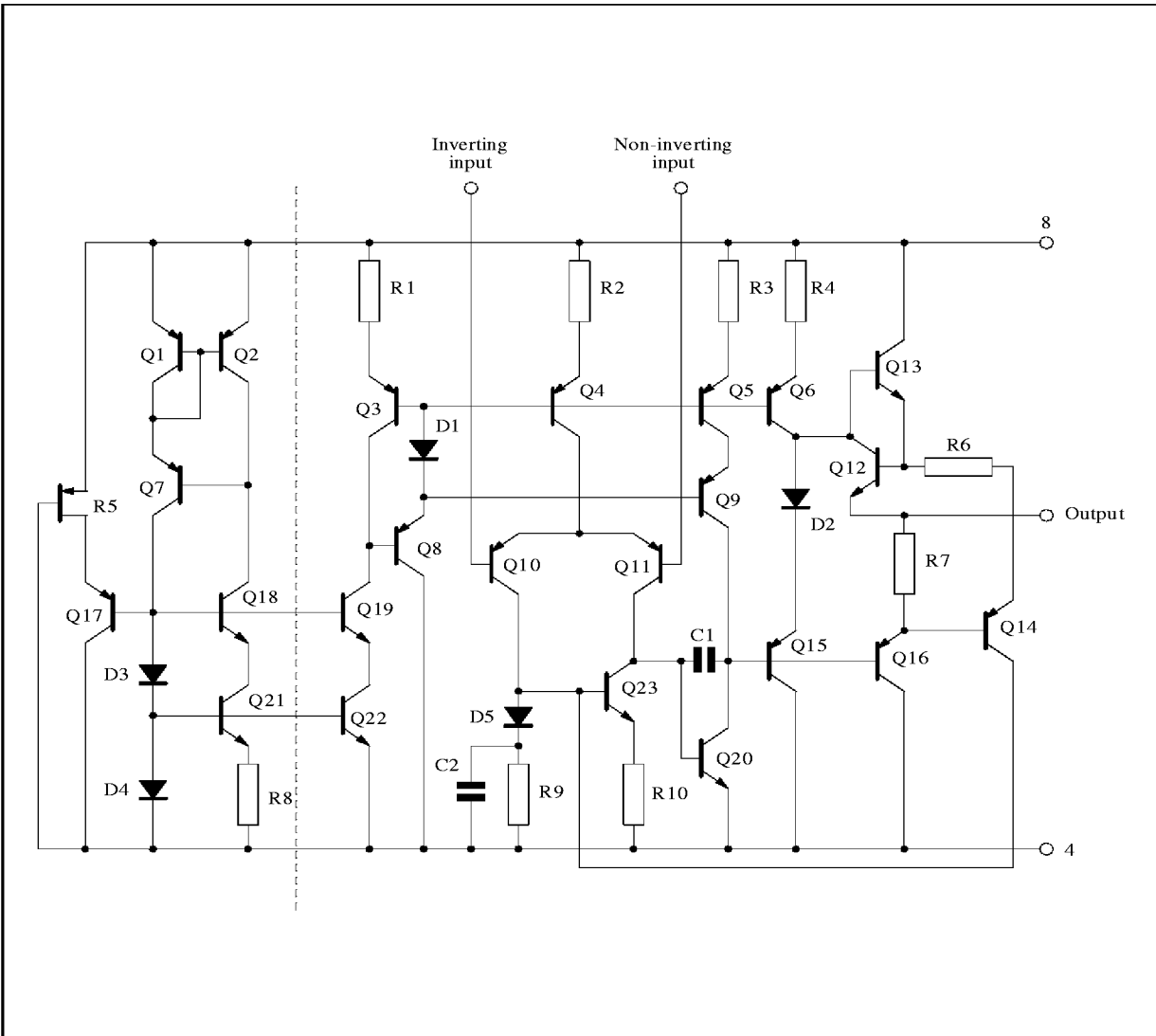
### ORDER CODES

Part Number	Temperature Range	Package	
		N	D
LS204C	0°C, +70°C	•	•
LS204I	-40°C, +105°C	•	•
LS204M	-55°C, +125°C	•	•

### PIN CONNECTIONS (top view)



SCHEMATIC DIAGRAM (1/2 LS204)



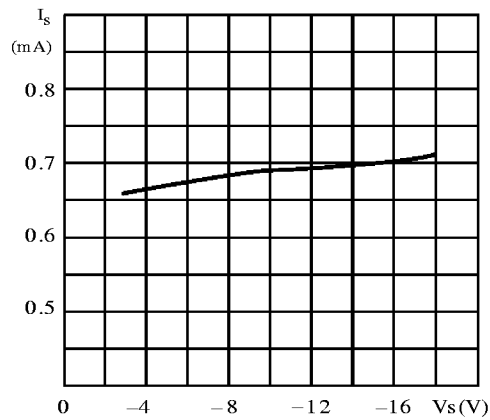
ABSOLUTE MAXIMUM RATINGS

Symbol	Parameter	Value	Unit
$V_{CC}$	Supply Voltage	$\pm 18$	V
$V_i$	Input Voltage	$\pm V_{CC}$	
$V_{id}$	Differential Input Voltage	$\pm (V_{CC} - 1)$	
$T_{oper}$	Operating Temperature Range	LS204C LS204I LS204M 0 to +70 -40 to +105 -55 to +125	$^{\circ}\text{C}$
$P_{tot}$	Power Dissipation at $T_{amb} = 70^{\circ}\text{C}$	500	mW
$T_j$	Junction Temperature	150	$^{\circ}\text{C}$
$T_{stg}$	Storage Temperature	-65 to 150	$^{\circ}\text{C}$

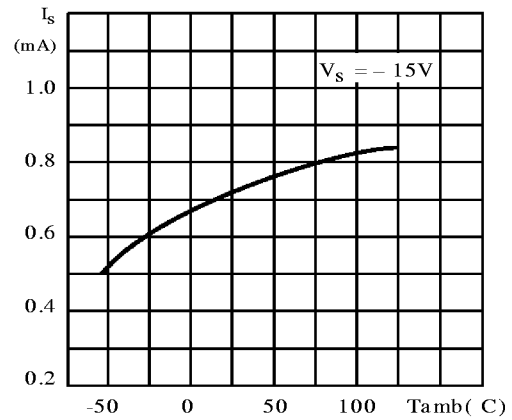
**ELECTRICAL CHARACTERISTICS** ( $V_{CC} = \pm 15V$ ,  $T_{amb} = 25^{\circ}C$ , unless otherwise specified)

Symbol	Parameter	Test Conditions	LS204I - LS204M			LS204C			Unit
			Min.	Typ.	Max.	Min.	Typ.	Max.	
$I_{CC}$	Supply Current			0.7	1.2		0.8	1.5	mA
$I_{ib}$	Input Bias Current	$T_{min.} < T_{op} < T_{max.}$		50	150		100	300	nA
					300			700	nA
$R_i$	Input Resistance	$f = 1kHz$		1			0.5		M $\Omega$
$V_{io}$	Input Offset Voltage	$R_s \leq 10k\Omega$		0.5	2.5		0.5	3.5	mV
		$R_s \leq 10k\Omega$ $T_{min.} < T_{op} < T_{max.}$			3.5			5	mV
$DV_{io}$	Input Offset Voltage Drift	$R_s \leq 10k\Omega$ $T_{min.} < T_{op} < T_{max.}$		5			5		$\mu V/^{\circ}C$
$I_{io}$	Input Offset Current	$T_{min.} < T_{op} < T_{max.}$		5	20		12	50	nA
					40			100	nA
$DI_{io}$	Input Offset Current Drift	$T_{min.} < T_{op} < T_{max.}$		0.08			0.1		$\frac{nA}{^{\circ}C}$
$I_{os}$	Output Short Circuit Current			23			23		mA
$A_{vd}$	Large Signal Voltage Gain	$T_{min.} < T_{op} < T_{max.}$ $R_L = 2k\Omega$ $V_{CC} = \pm 15V$ $V_{CC} = \pm 4V$	90	100 95		86	100 95		dB
GBP	Gain-bandwidth Product	$f = 100kHz$	1.8	3		1.5	2.5		MHz
$e_n$	Equivalent Input Noise Voltage	$f = 1kHz$ $R_s = 50\Omega$ $R_s = 1k\Omega$ $R_s = 10k\Omega$		8 10 18	15		10 12 20		$\frac{nV}{\sqrt{Hz}}$
THD	Total Harmonic Distortion	$A_V = 20dB$ $R_L = 2k\Omega$ $V_O = 2V_{PP}$ $f = 1kHz$		0.03	0.1		0.03	0.1	%
$\pm V_{opp}$	Output Voltage Swing	$R_L = 2k\Omega$ $V_{CC} = \pm 15V$ $V_{CC} = \pm 4V$	$\pm 13$	$\pm 3$		$\pm 13$	$\pm 3$		V
$V_{opp}$	Large Signal Voltage Swing	$R_L = 10k\Omega$ $f = 10kHz$		28			28		$V_{PP}$
SR	Slew Rate	Unity Gain, $R_L = 2k\Omega$	0.8	1.5			1		V/ $\mu s$
CMR	Common Mode Rejection Ratio	$V_{ic} = 10V$ $T_{min.} < T_{op} < T_{max.}$	90			86			dB
SVR	Supply Voltage Rejection Ratio	$V_{ic} = 1V$ $f = 100Hz$ $T_{min.} < T_{op} < T_{max.}$	90			86			dB
$V_{O1}/V_{O2}$	Channel Separation	$f = 1kHz$	100	120			120		dB

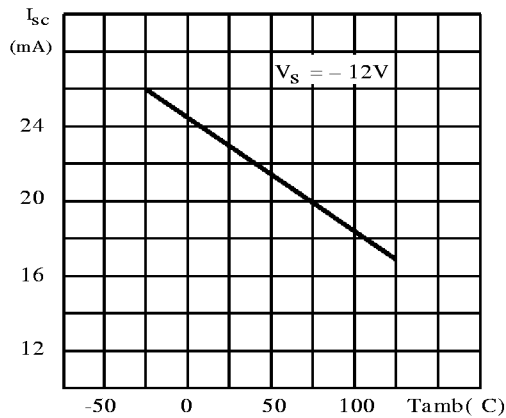
**Figure 1 :** Supply Current versus Supply Voltage



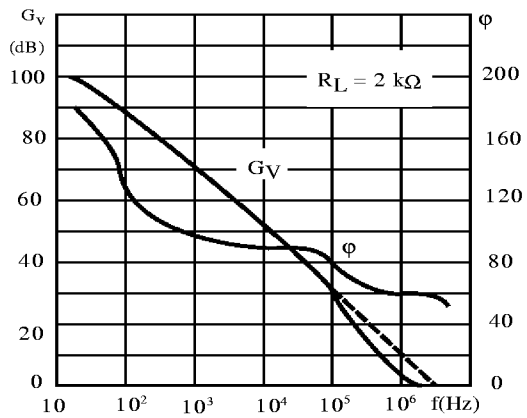
**Figure 2 :** Supply Current versus Ambient Temperature



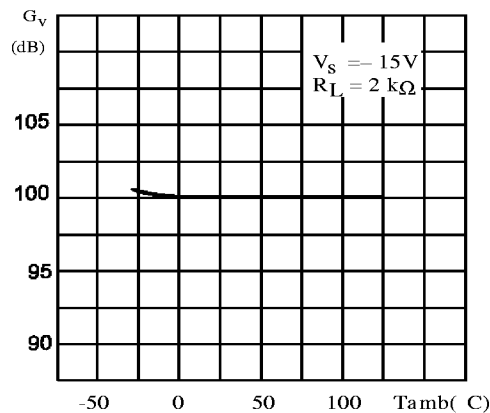
**Figure 3 :** Output Short Circuit Current versus Ambient Temperature



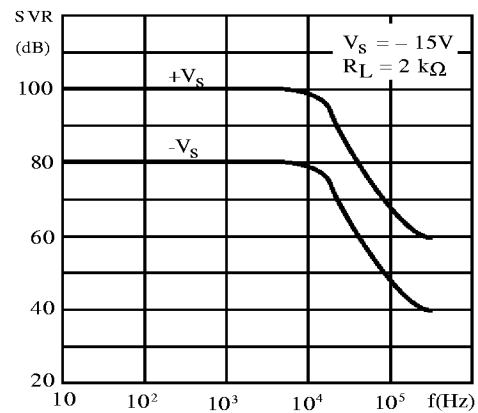
**Figure 4 :** Open Loop Frequency and Phase Response

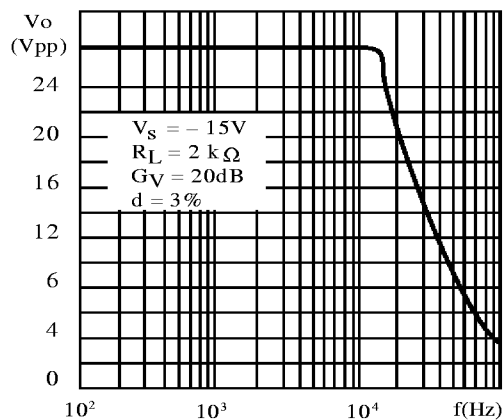
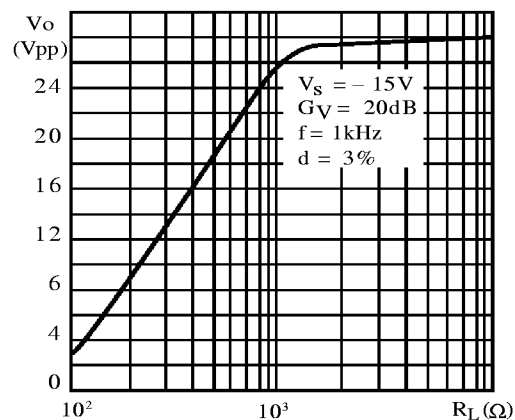
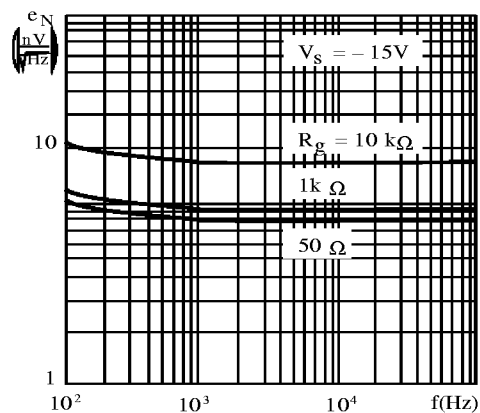
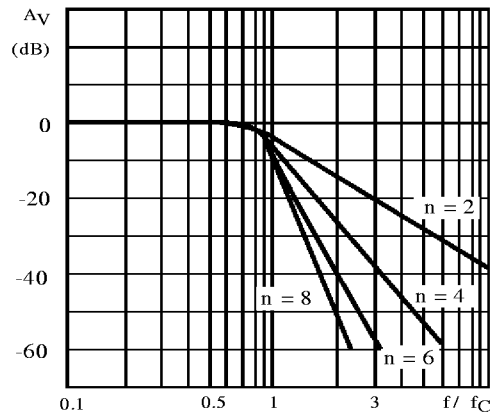
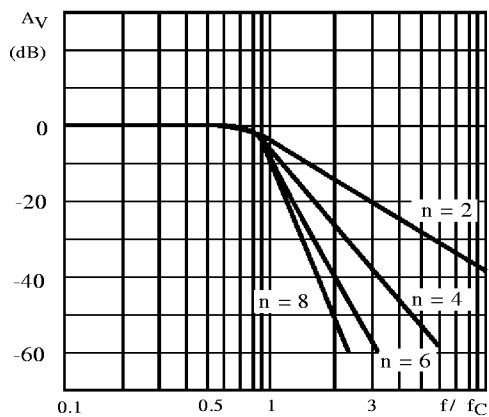
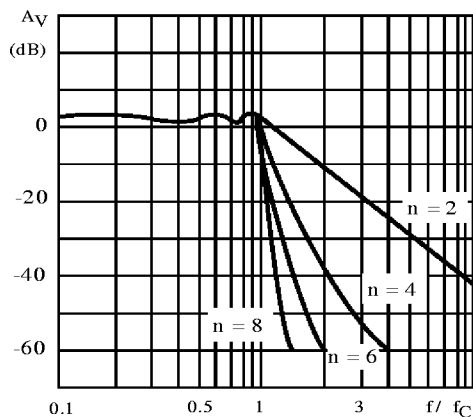


**Figure 5 :** Output Loop Gain versus Ambient Temperature



**Figure 6 :** Supply Voltage Rejection versus Frequency



**Figure 7 : Large Signal Frequency Response****Figure 8 : Output Voltage Swing versus Load Resistance****Figure 9 : Total Input Noise versus Frequency****Figure 10 : Amplitude Response****Figure 11 : Amplitude Response****Figure 12 : Amplitude Response ( $\pm 1\text{dB}$  ripple)**

**APPLICATION INFORMATION : Active low-pass filter****BUTTERWORTH**

The Butterworth is a "maximally flat" amplitude response filter. Butterworth filters are used for filtering signals in data acquisition systems to prevent aliasing errors in sampled-data applications and for general purpose low-pass filtering.

The cut-off frequency  $f_c$ , is the frequency at which the amplitude response is down 3dB. The attenuation rate beyond the cutoff frequency is  $n$  dB per octave of frequency where  $n$  is the order (number of poles) of the filter.

Other characteristics :

- Flattest possible amplitude response.
- Excellent gain accuracy at low frequency end of passband.

**BESSEL**

The Bessel is a type of "linear phase" filter. Because of their linear phase characteristics, these filters approximate a constant time delay over a limited frequency range. Bessel filters pass transient waveforms with a minimum of distortion. They are also used to provide time delays for low pass filtering of modulated waveforms and as a "running average" type filter.

The maximum phase shift is  $\frac{-n\pi}{2}$  radians where  $n$  is the order (number of poles) of the filter. The cut-off frequency  $f_c$ , is defined as the frequency at which the phase shift is one half of this value. For accurate delay, the cut-off frequency should be twice the

maximum signal frequency.

The following table can be used to obtain the -3dB frequency of the filter.

	2 pole	4 Pole	6 Pole	8 Pole
-3dB Frequency	$0.77f_c$	$0.67f_c$	$0.57f_c$	$0.50f_c$

Other characteristics :

- Selectivity not as great as Chebyshev or Butterworth.
- Very little overshoot response to step inputs.
- Fast rise time.

**CHEBYSCHEV**

Chebyshev filters have greater selectivity than either Bessel or Butterworth at the expense of ripple in the passband.

Chebyshev filters are normally designed with peak-to-peak ripple values from 0.2dB to 2dB.

Increased ripple in the passband allows increased attenuation above the cut-off frequency.

The cut-off frequency is defined as the frequency at which the amplitude response passes through the specified maximum ripple band and enters the stop band.

Other characteristics :

- Greater selectivity
- Very non-linear phase response
- High overshoot response to step inputs

The table below shows the typical overshoot and settling time response of the low pass filters to a step input.

	Number of Poles	Peak Overshoot	Settling Time (% of final value)		
		% Overshoot	$\pm 1\%$	$\pm 0.1\%$	$\pm 0.01\%$
Butterworth	2	4	$1.1/f_c \text{ sec.}$	$1.7/f_c \text{ sec.}$	$1.9/f_c \text{ sec.}$
	4	11	$1.7/f_c$	$2.8/f_c$	$3.8/f_c$
	6	14	$2.4/f_c$	$3.9/f_c$	$5.0/f_c$
	8	16	$3.1/f_c$	$5.1/f_c$	$7.1/f_c$
Bessel	2	0.4	$0.8/f_c$	$1.4/f_c$	$1.7/f_c$
	4	0.8	$1.0/f_c$	$1.8/f_c$	$2.4/f_c$
	6	0.6	$1.3/f_c$	$2.1/f_c$	$2.7/f_c$
	8	0.3	$1.6/f_c$	$2.3/f_c$	$3.2/f_c$
Chebyshev (ripple $\pm 0.25\text{dB}$ )	2	11	$1.1/f_c$	$1.6/f_c$	—
	4	18	$3.0/f_c$	$5.4/f_c$	—
	6	21	$5.9/f_c$	$10.4/f_c$	—
	8	23	$8.4/f_c$	$16.4/f_c$	—
Chebyshev (ripple $\pm 1\text{dB}$ )	2	21	$1.6/f_c$	$2.7/f_c$	—
	4	28	$4.8/f_c$	$8.4/f_c$	—
	6	32	$8.2/f_c$	$16.3/f_c$	—
	8	34	$11.6/f_c$	$24.8/f_c$	—

Design of 2nd order active low pass filter (Sallen and Key configuration unity gain op-amp)

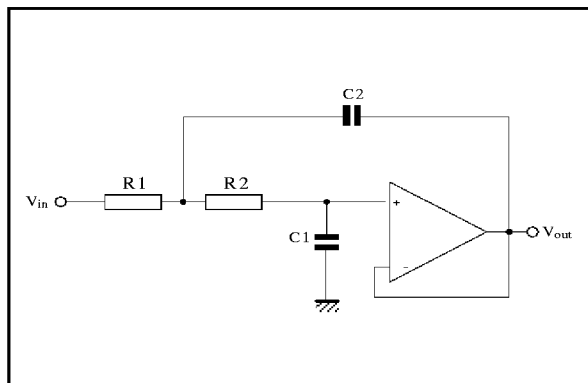
Fixed  $R = R_1 = R_2$ , we have (see fig. 13).

$$C_1 = \frac{1}{R} \frac{\xi}{\omega_c}$$

$$C_2 = \frac{1}{R} \frac{1}{\xi \omega_c}$$

The diagram of fig.14 shows the amplitude response for different values of damping factor  $\xi$  in 2nd order filters.

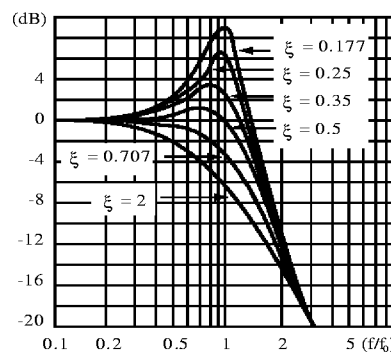
**Figure 13 : Filter Configuration**



Three parameters are needed to characterize the frequency and phase response of a 2<sup>nd</sup> order active filter : the gain ( $G_v$ ), the damping factor ( $\xi$ ) or the Q-factor ( $Q = (2\xi)^{-1}$ ), and the cutoff frequency ( $f_c$ ).

The higher order responses are obtained with a se-

**Figure 14 : Filter Respons versus Damping Factor**



ries of 2<sup>nd</sup> order sections. A simple RC section is introduced when an odd filter is required.

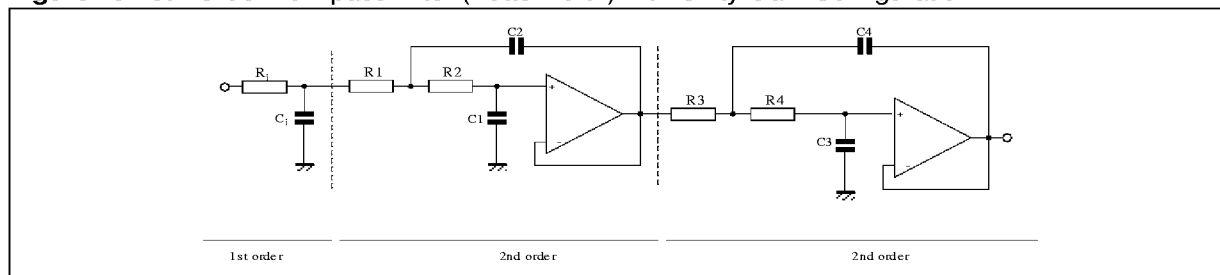
The choice of ' $\xi$ ' (or Q-factor) determines the filter response (see table 1).

**Table 1**

Filter Response	$\xi$	Q	Cutoff Frequency $f_c$
Bessel	$\frac{\sqrt{3}}{2}$	$\frac{\sqrt{1}}{3}$	Frequency at which Phase Shift is $-90^\circ$ C
Butterworth	$\frac{\sqrt{2}}{2}$	$\frac{\sqrt{1}}{2}$	Frequency at which $G_v = -3$ dB
Chebyshev	$\frac{\sqrt{2}}{2}$	$\frac{\sqrt{1}}{2}$	Frequency at which the amplitude response passes through specified max. ripple band and enters the stop band.

### EXAMPLE

**Figure 15 : 5th Order Low-pass Filter (Butterworth) with Unity Gain Configuration**



In the circuit of fig. 15, for  $f_c = 3.4\text{kHz}$  and  $R_i = R_1 = R_2 = R_3 = R_4 = 10\text{k}\Omega$ , we obtain :

$$C_i = 1.354 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 6.33\text{nF}$$

$$C_1 = 0.421 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 1.97\text{nF}$$

$$C_2 = 1.753 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 8.20\text{nF}$$

$$C_3 = 0.309 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 1.45\text{nF}$$

$$C_4 = 3.325 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 15.14\text{nF}$$

The attenuation of the filter is 30dB at 6.8kHz and better than 60dB at 15kHz.

The same method, referring to Tab. 2 and fig. 16, is used to design high-pass filter. In this case the damping factor is found by taking the reciprocal of the numbers in Tab. 2. For  $f_c = 5\text{kHz}$  and  $C_i = C_1 = C_2 = C_3 = C_4 = 1\text{nF}$  we obtain :

$$R_i = \frac{1}{0.354} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 25.5\text{k}\Omega$$

$$R_1 = \frac{1}{0.421} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 75.6\text{k}\Omega$$

$$R_2 = \frac{1}{1.753} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 18.2\text{k}\Omega$$

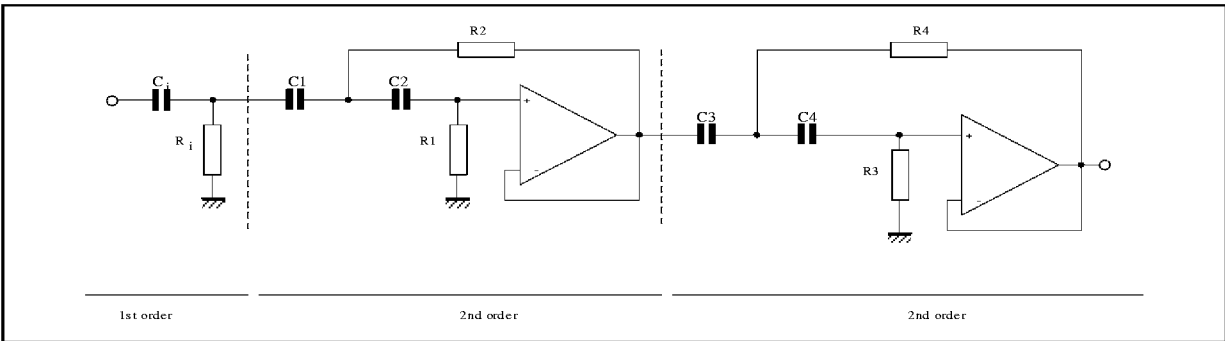
$$R_3 = \frac{1}{0.309} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 103\text{k}\Omega$$

$$R_4 = \frac{1}{3.325} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 9.6\text{k}\Omega$$

**Table 2** : Damping Factor for Low-pass Butterworth Filters

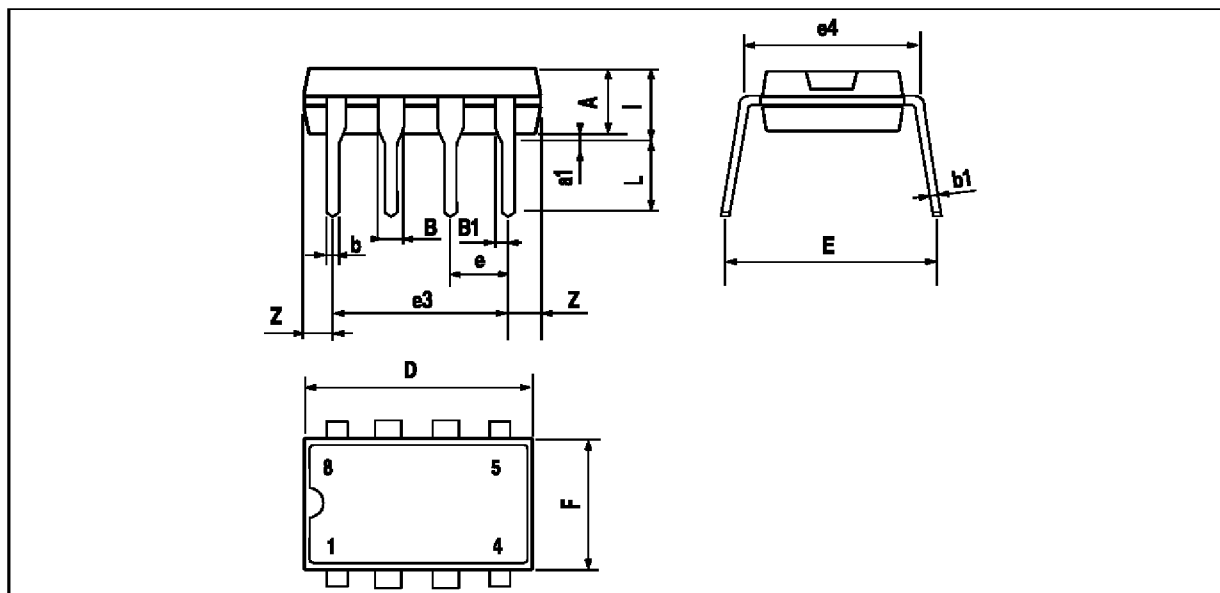
Order	C <sub>i</sub>	C <sub>1</sub>	C <sub>2</sub>	C <sub>3</sub>	C <sub>4</sub>	C <sub>5</sub>	C <sub>6</sub>	C <sub>7</sub>	C <sub>8</sub>
2		0.707	1.41						
3	1.392	0.202	3.54						
4		0.92	1.08	0.38	2.61				
5	1.354	0.421	1.75	0.309	3.235				
6		0.966	1.035	0.707	1.414	0.259	3.86		
7	1.336	0.488	1.53	0.623	1.604	0.222	4.49		
8		0.98	1.02	0.83	1.20	0.556	1.80	0.195	5.125

**Figure 16** : 5th Order High-pass Filter (Butterworth) with Unity Gain Configuration





# **PACKAGE MECHANICAL DATA** **8 PINS - PLASTIC DIP**

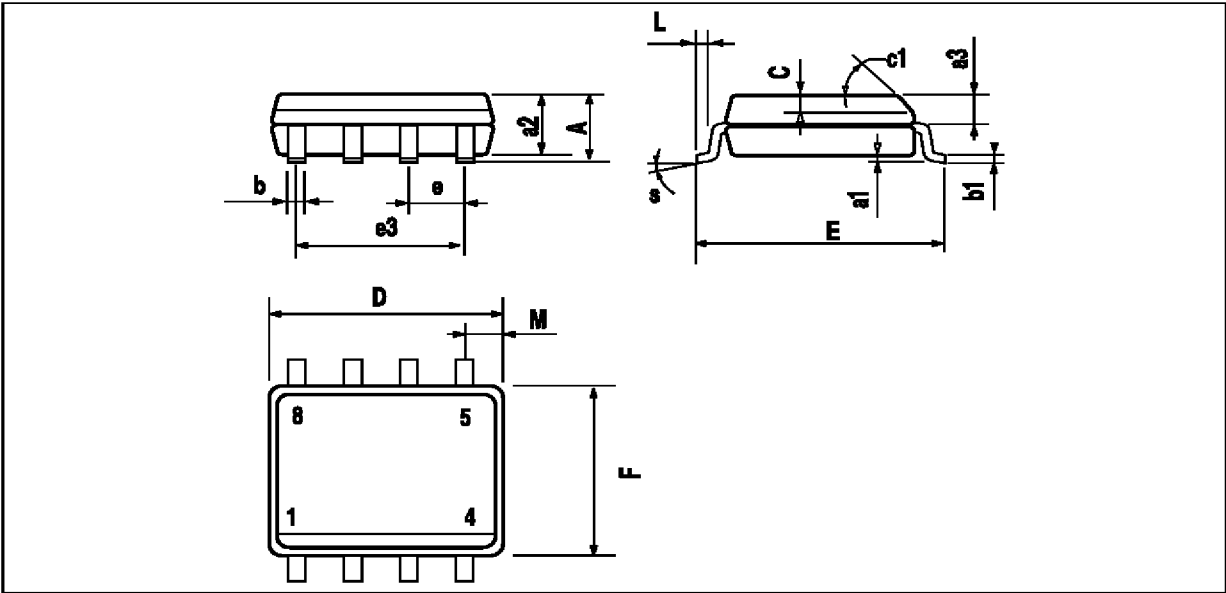


P440P4EFS

Dimensions	Millimeters			Inches		
	Min.	Typ.	Max.	Min.	Typ.	Max.
A		3.32			0.131	
a1	0.51			0.020		
B	1.15		1.65	0.045		0.065
b	0.356		0.55	0.014		0.022
b1	0.204		0.304	0.008		0.012
D			10.92			0.430
E	7.95		9.75	0.313		0.384
e		2.54			0.100	
e3		7.62			0.300	
e4		7.62			0.300	
F			6.6			0.260
i			5.08			0.200
L	3.18		3.81	0.125		0.150
Z			1.52			0.060

DPA8 TEL

PACKAGE MECHANICAL DATA  
8 PINS - PLASTIC MICROPACKAGE (SO)



Dimensions	Millimeters			Inches		
	Min.	Typ.	Max.	Min.	Typ.	Max.
A			1.75			0.069
a1	0.1		0.25	0.004		0.010
a2			1.65			0.065
a3	0.65		0.85	0.026		0.033
b	0.35		0.48	0.014		0.019
b1	0.19		0.25	0.007		0.010
C	0.25		0.5	0.010		0.020
c1	45° (typ.)					
D	4.8		5.0	0.189		0.197
E	5.8		6.2	0.228		0.244
e		1.27			0.050	
e3		3.81			0.150	
F	3.8		4.0	0.150		0.157
L	0.4		1.27	0.016		0.050
M			0.6			0.024
S	8° (max.)					

Information furnished is believed to be accurate and reliable. However, SGS-THOMSON Microelectronics assumes no responsibility for the consequences of use of such information nor for any infringement of patents or other rights of third parties which may result from its use. No licence is granted by implication or otherwise under any patent or patent rights of SGS-THOMSON Microelectronics. Specifications mentioned in this publication are subject to change without notice. This publication supersedes and replaces all information previously supplied. SGS-THOMSON Microelectronics products are not authorized for use as critical components in life support devices or systems without express written approval of SGS-THOMSON Microelectronics.

© 1995 SGS-THOMSON Microelectronics - All Rights Reserved

SGS-THOMSON Microelectronics GROUP OF COMPANIES

Australia - Brazil - France - Germany - Hong Kong - Italy - Japan - Korea - Malaysia - Malta - Morocco - The Netherlands  
Singapore - Spain - Sweden - Switzerland - Taiwan - Thailand - United Kingdom - U.S.A.