

# AN11228

## BGA301x Wideband Variable Gain Amplifier Application

Rev. 2 — 3 February 2014

Application note

### Document information

Info	Content
<b>Keywords</b>	BGA3015, BGA3018, BAP70Q, CATV, Line-up, VGA, Evaluation board
<b>Abstract</b>	This application note describes the schematic and layout requirements for using the BGA3015 and BGA3018 drop amplifiers together with the BAP70Q quad pin diode in a CATV VGA application.



## Revision history

Rev	Date	Description
2	20140203	Updated with improved application circuit and test data
1	20121012	First version

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## 1. Introduction

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With the use of NXP's BGA301x drop amplifiers and the BAP70Q quad pin diode attenuator a wideband Variable Gain Amplifier (VGA) has been made which can be used as line-up amplifier in CATV networks.

The combination of NXP's BGA301x amplifiers and BAP70Q pin diode parts a high gain amplifier with low noise figure and wide dynamic range can be made.

This application note describes the evaluation board schematic and layout requirements, and shows the test results.

## 2. System features

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- 75  $\Omega$  input and output impedance
- Gain control dynamic range of 20 dB
- Flat gain between 40 MHz and 1003 MHz
- Unconditionally stable
- Excellent input and output return loss

## 3. Customer evaluation kit contents

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The evaluation kit contains the following items:

- ESD safe casing
- BGA301x VGA evaluation board

## 4. Application information

The evaluation circuit can be seen in figure 1 and the corresponding PCB is shown in figure 2. Table 1 shows the bill of materials.

### 4.1 Evaluation board circuit

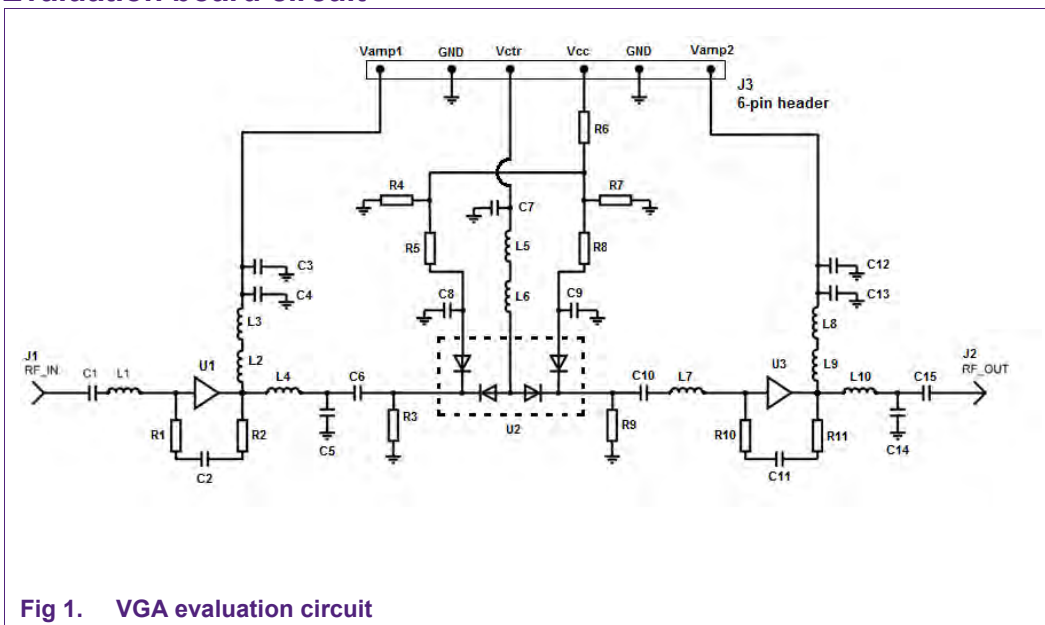


Fig 1. VGA evaluation circuit

The connector pinning is as followed:

- "GND" : Ground pins
- "Vamp1" : +8 V power supply for amplifier U1
- "Vamp2" : +8 V power supply for amplifier U3
- "Vcc" : +8 V power supply for pin diode attenuator U2
- "Vctr" : Pin diode attenuator control voltage (1 ... 3 V)

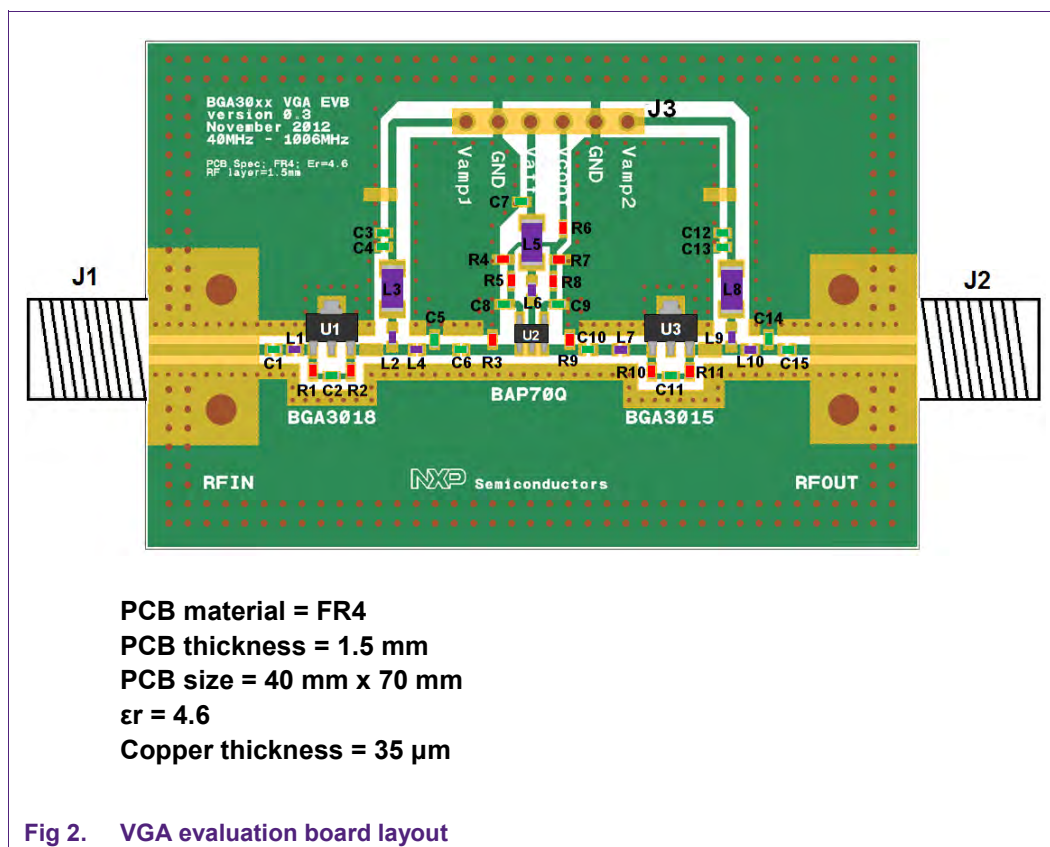
At connector J1 the RF signal from an external optical receiver is applied, where C1 provides DC-blocking, followed by L1 for S11 matching of the BGA3018 amplifier (U1).

The feedback of amplifier U1 is provided via R1 & R2 with C2 for DC-blocking between the input and output pins of the amplifier. Two resistors are used to lower the influence of the parasitic capacitance from the circuit board. The output of amplifier U1 is matched with L4 and C6 provides the DC-blocking towards pin-diode attenuator U2.

The signal out of the first amplifier has a large dynamic range and with use of the BAP70Q pin diode attenuator (U2) the RF signals can be attenuated in such a way that a stable RF signal will be available at the output of the pin-diode attenuator. The stable output signal is amplified again by the BGA3015 amplifier (U3).

C10 provides DC-blocking, followed by L7 for S11 matching of the BGA3015 amplifier (U3). The feedback of amplifier U2 is provided via R10 & R11 with C11 for DC-blocking between the input and the output pins of the amplifier. Two resistors are used to lower the influence of the parasitic capacitance from the circuit board. The output of amplifier U3 is matched with L10 and C15 provides the DC-blocking towards the output connector J2.

## 4.2 Evaluation board layout



For optimum distortion performance it is important to have enough ground vias underneath and around the MMICs ground pins. This lowers the inductance to the ground plane. The evaluation board is made with two layer FR4 material.

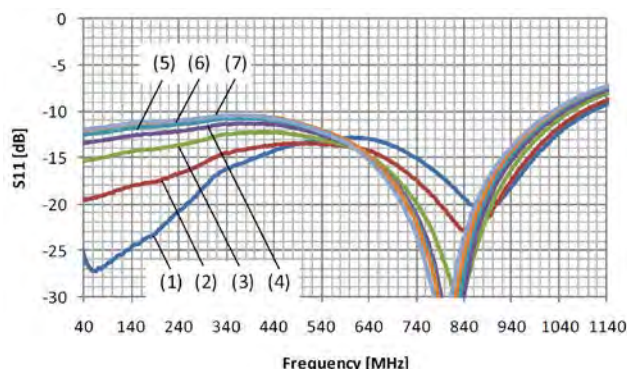
### 4.3 Bill of materials

**Table 1. Evaluation board BoM**

Circuit reference	Description	Qty	Mfr	Manufacturer number	Supplier	Supplier part number
U1	BGA3018	1	NXP	BGA3018	NXP	BGA3018
U2	BAP70Q	1	NXP	BAP70Q	NXP	BAP70Q
U3	BGA3015	1	NXP	BGA3015	NXP	BGA3015
C1, C2, C3 C6, C7, C8 C9, C11, C12 C15	10 nF	10	Murata	GRM155R71E103KA01D	Digikey	490-1312-1-ND
C4, C13	100 pF	2	Murata	GRM1555C1H101JZ01D	Digikey	490-3458-1-ND
C10	270 pF	1	Murata	GRM1555C1H271JA01D	Digikey	490-1294-1-ND
C5	-	-	-	-	-	-
C14	-	-	-	-	-	-
L1, L10	3.9 nH	2	Murata	LQG15HS3N9S02D	Digikey	490-2617-1-ND
L4	8.2 nH	1	Murata	LQG15HN8N2J02D	Digikey	490-2622-1-ND
L2, L6, L9	Choke	3	Murata	BLM15HD182SN1D	Digikey	490-5196-1-ND
L3, L5, L8	880 nH	3	Murata	LQH31HNR88K03L	Digikey	LQH31HNR88K03 L-ND
L7	0 $\Omega$ (Jumper)	1	Yageo	RC0402FR-070RL	Digikey	311-0.0LRCT-ND
R1, R3, R9	470 $\Omega$	3	Yageo	RC0402FR-07470RL	Digikey	311-470LRCT-ND
R2, R10, R11	300 $\Omega$	3	Yageo	RC0402FR-07300RL	Digikey	311-300LRCT-ND
R5, R8	0 $\Omega$ (Jumper)	2	Yageo	RC0402FR-070RL	Digikey	311-0.0LRCT-ND
R4, R7	1200 $\Omega$	2	Yageo	RC0402FR-71K2L	Digikey	311-1.20KLRCT-ND
R6	2200 $\Omega$	1	Yageo	RC0402FR-72K2L	Digikey	311-2.20KLRCT-ND
J1, J2	75 $\Omega$ F-connector	2	Bomar	861V509ER6	Mouser	678-861V509ER6
J3	Header 6	1	Molex	90121-0766	Digikey	WM8112-ND

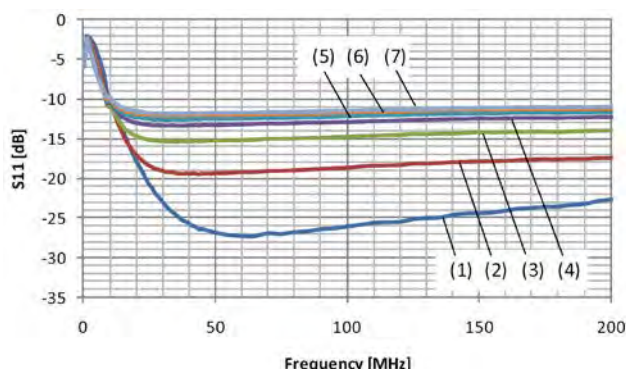
## 5. Measurement results at $V_{CC} = 8\text{ V}$

### 5.1 S-Parameters



a. S11: 40 MHz – 1140 MHz

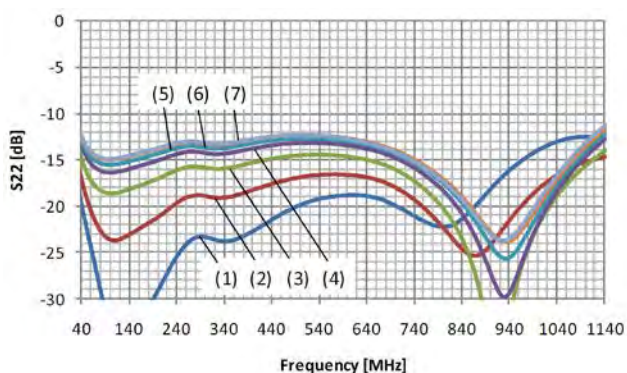
- (1):  $V_{ctr} = 2.13\text{ V}$
- (2):  $V_{ctr} = 1.80\text{ V}$
- (3):  $V_{ctr} = 1.64\text{ V}$
- (4):  $V_{ctr} = 1.50\text{ V}$
- (5):  $V_{ctr} = 1.39\text{ V}$
- (6):  $V_{ctr} = 1.29\text{ V}$
- (7):  $V_{ctr} = 1.12\text{ V}$



b. S11: 300 kHz – 200 MHz

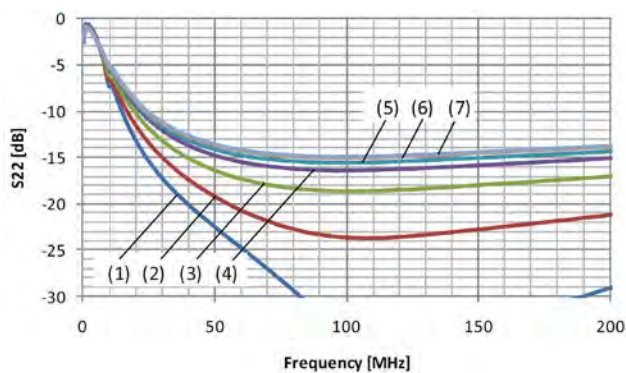
- (1):  $V_{ctr} = 2.13\text{ V}$
- (2):  $V_{ctr} = 1.80\text{ V}$
- (3):  $V_{ctr} = 1.64\text{ V}$
- (4):  $V_{ctr} = 1.50\text{ V}$
- (5):  $V_{ctr} = 1.39\text{ V}$
- (6):  $V_{ctr} = 1.29\text{ V}$
- (7):  $V_{ctr} = 1.12\text{ V}$

**Fig 3. Input matching (S11);  $V_{CC} = 8\text{ V}$**



a. S22: 40 MHz – 1140 MHz

- (1):  $V_{ctr} = 2.13\text{ V}$
- (2):  $V_{ctr} = 1.80\text{ V}$
- (3):  $V_{ctr} = 1.64\text{ V}$
- (4):  $V_{ctr} = 1.50\text{ V}$
- (5):  $V_{ctr} = 1.39\text{ V}$
- (6):  $V_{ctr} = 1.29\text{ V}$
- (7):  $V_{ctr} = 1.12\text{ V}$

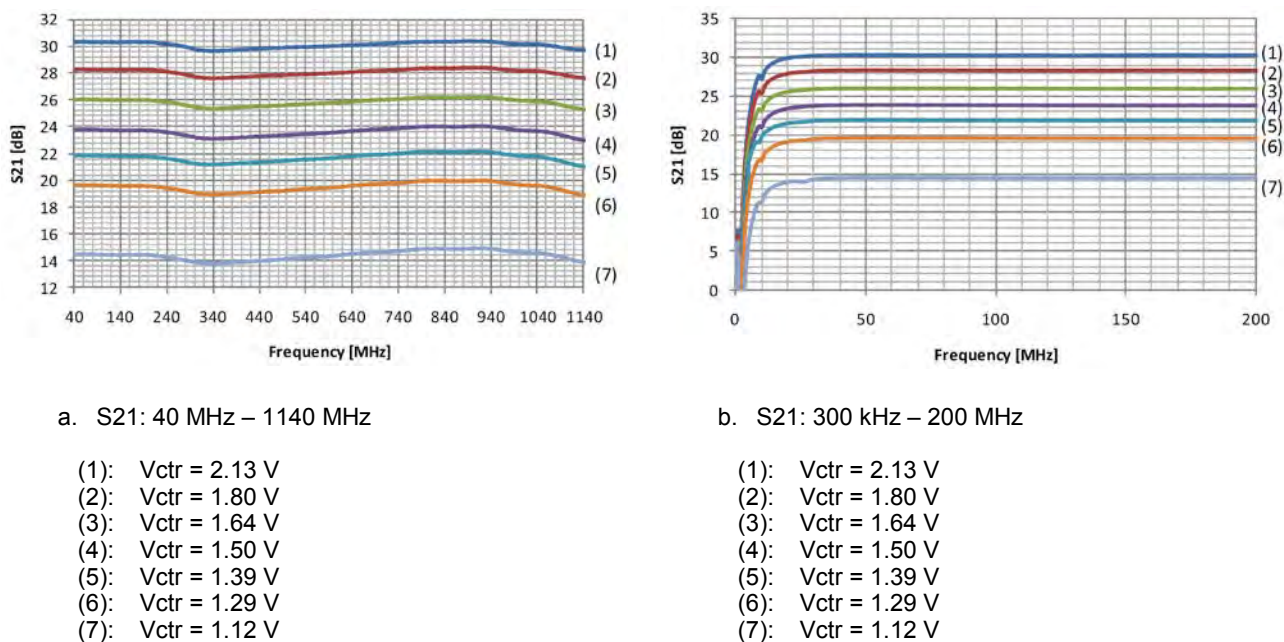
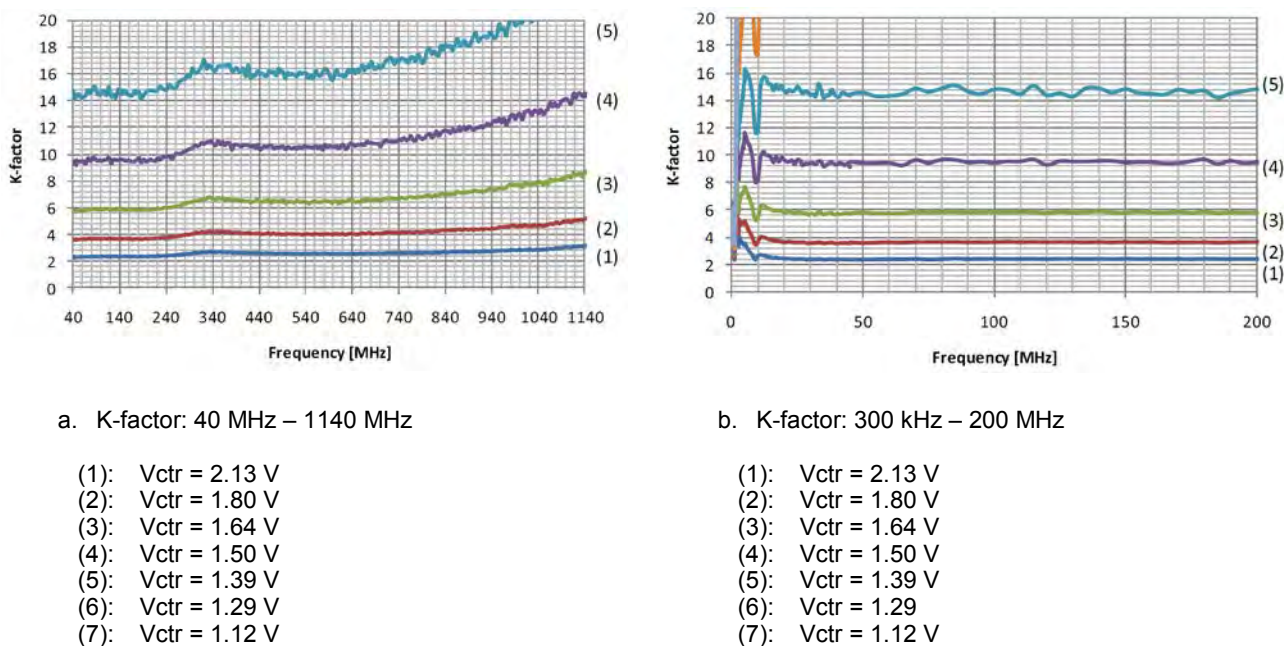


b. S22: 300 kHz – 200 MHz

- (1):  $V_{ctr} = 2.13\text{ V}$
- (2):  $V_{ctr} = 1.80\text{ V}$
- (3):  $V_{ctr} = 1.64\text{ V}$
- (4):  $V_{ctr} = 1.50\text{ V}$
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- (6):  $V_{ctr} = 1.29\text{ V}$
- (7):  $V_{ctr} = 1.12\text{ V}$

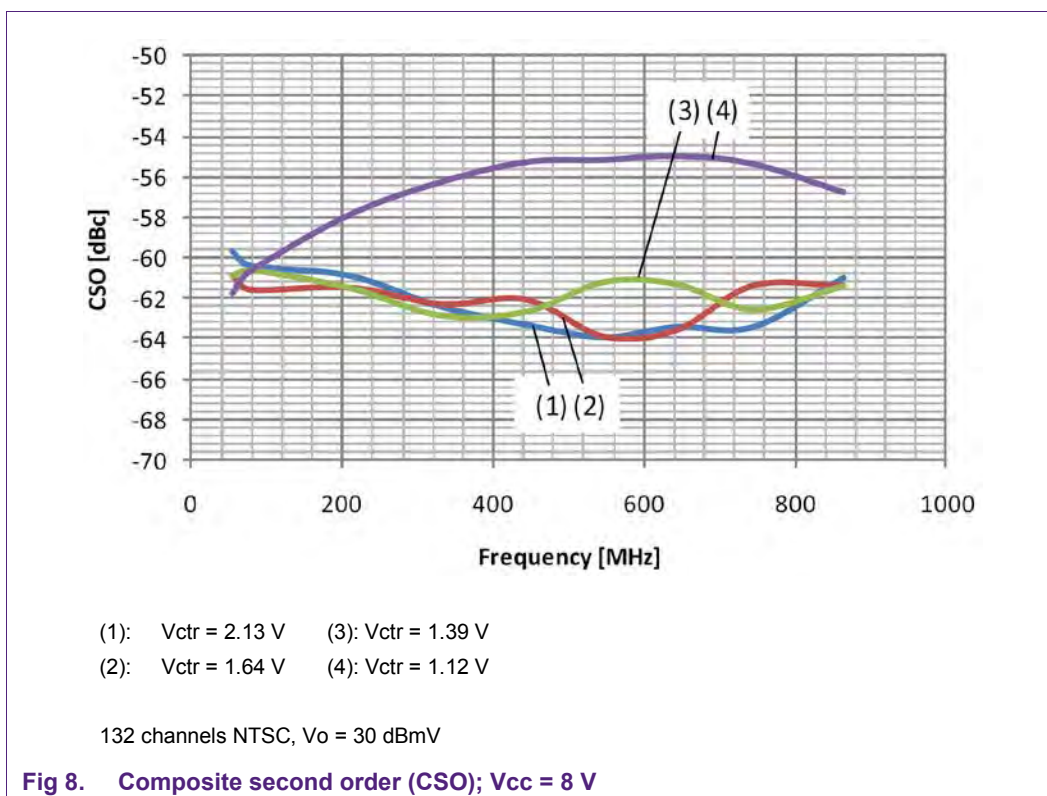
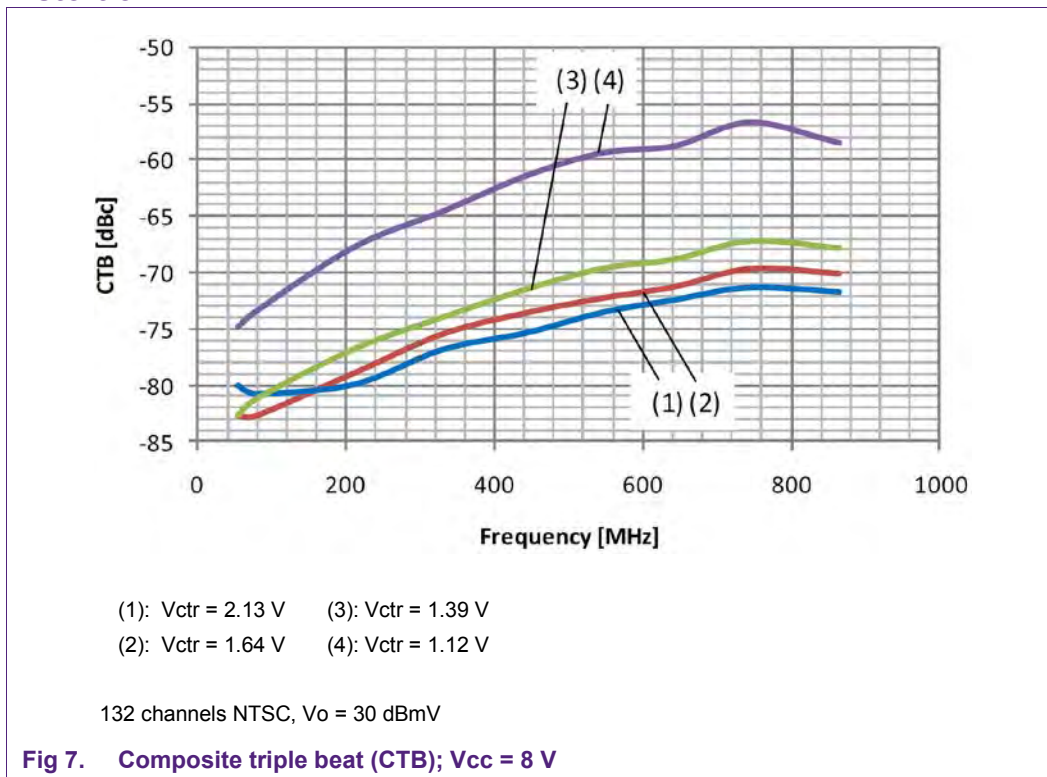
**Fig 4. Output matching (S22);  $V_{CC} = 8\text{ V}$**

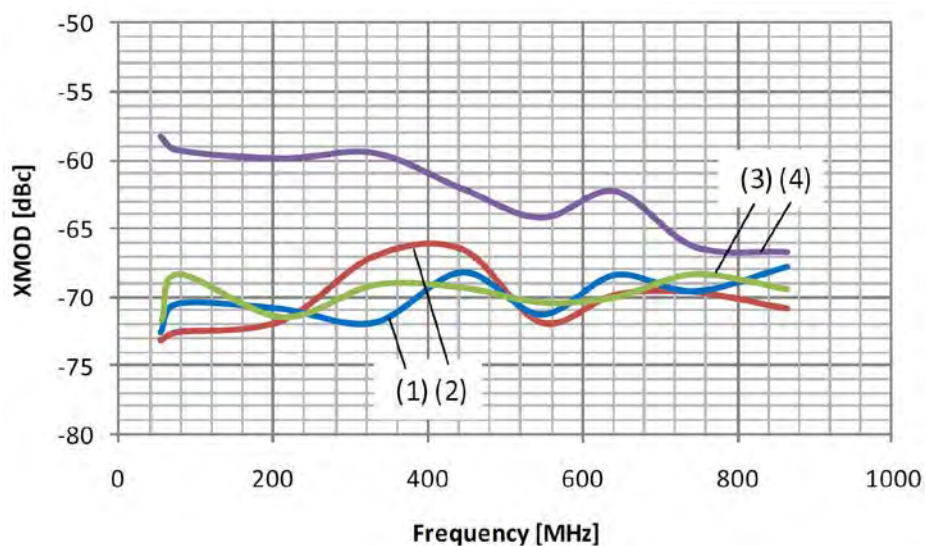


Fig 5. Gain ( $S_{21}$ );  $V_{cc} = 8$  VFig 6. K-factor; typical;  $V_{cc} = 8$  V



## 5.2 Distortion



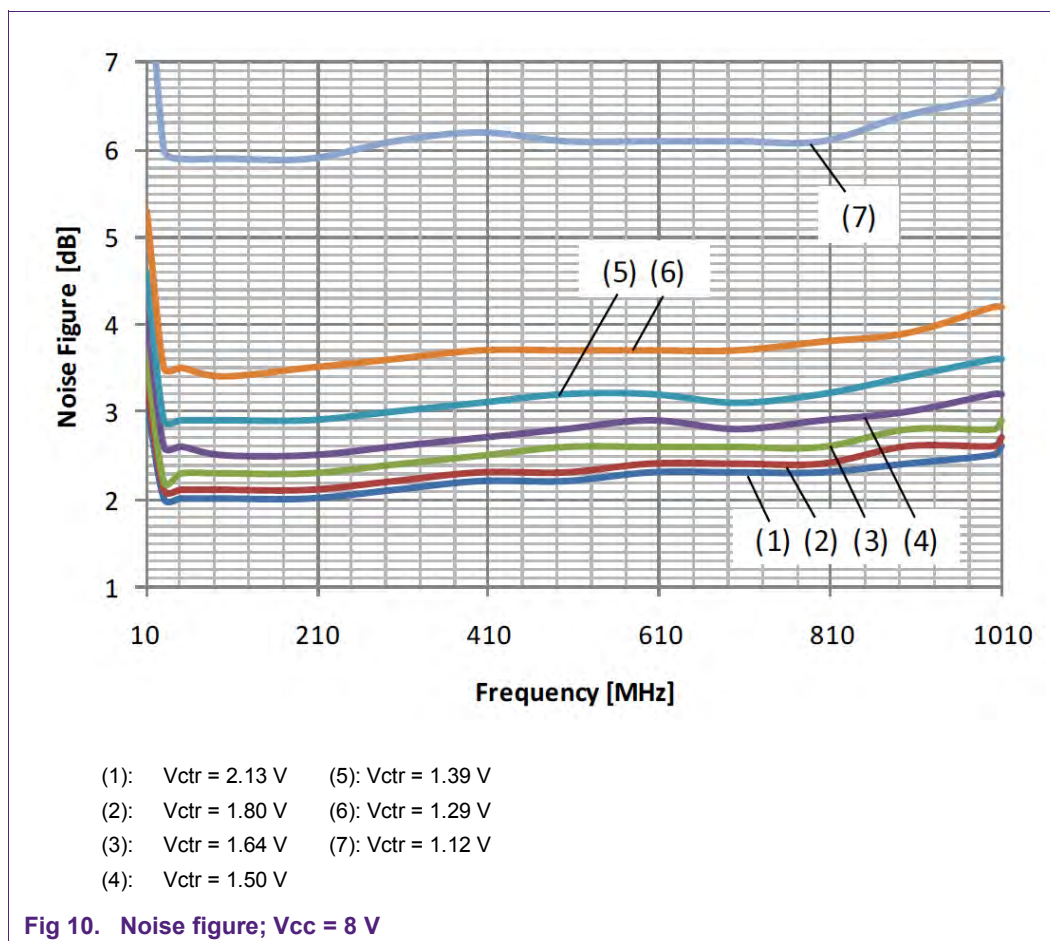


(1):  $V_{ctr} = 2.13 \text{ V}$  (3):  $V_{ctr} = 1.39 \text{ V}$   
(2):  $V_{ctr} = 1.64 \text{ V}$  (4):  $V_{ctr} = 1.12 \text{ V}$

132 channels NTSC,  $V_o = 30 \text{ dBmV}$

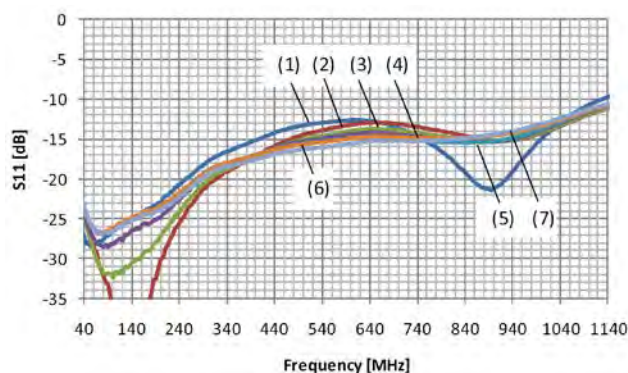
**Fig 9. Cross modulation (XMOD);  $V_{cc} = 8 \text{ V}$**

### 5.3 Noise figure



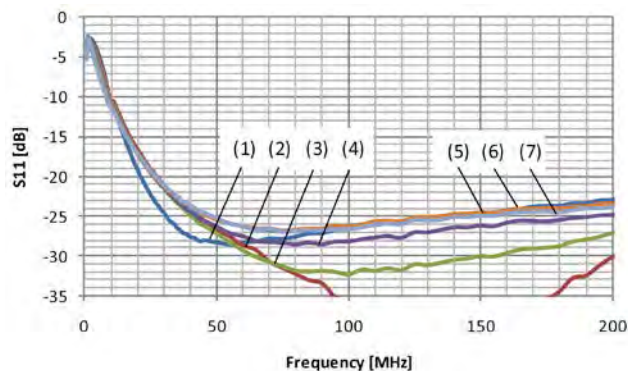
## 6. Measurement results at $V_{cc} = 5\text{ V}$

### 6.1 S-Parameters



a. S11: 40 MHz – 1140 MHz

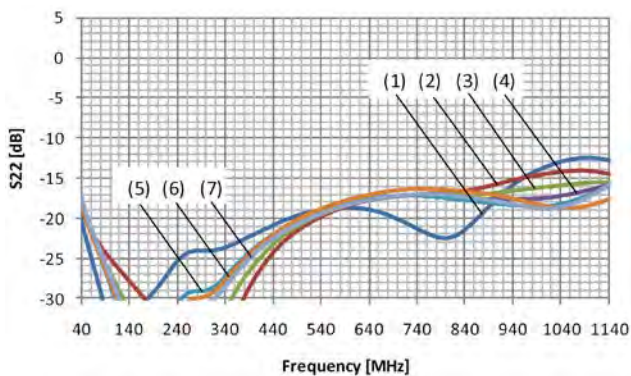
- (1):  $V_{ctr} = 2.13\text{ V}$
- (2):  $V_{ctr} = 1.80\text{ V}$
- (3):  $V_{ctr} = 1.64\text{ V}$
- (4):  $V_{ctr} = 1.50\text{ V}$
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- (6):  $V_{ctr} = 1.29\text{ V}$
- (7):  $V_{ctr} = 1.12\text{ V}$



b. S11: 300 kHz – 200 MHz

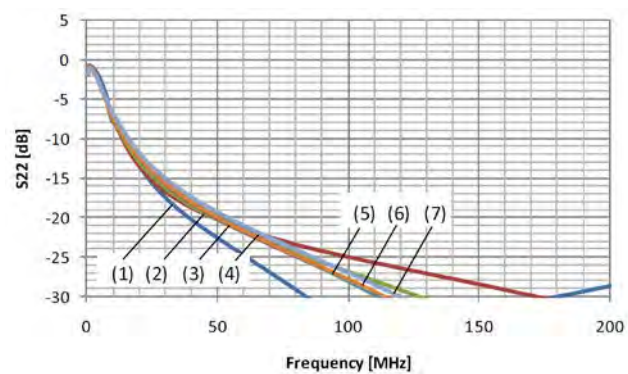
- (1):  $V_{ctr} = 2.13\text{ V}$
- (2):  $V_{ctr} = 1.80\text{ V}$
- (3):  $V_{ctr} = 1.64\text{ V}$
- (4):  $V_{ctr} = 1.50\text{ V}$
- (5):  $V_{ctr} = 1.39\text{ V}$
- (6):  $V_{ctr} = 1.29\text{ V}$
- (7):  $V_{ctr} = 1.12\text{ V}$

Fig 11. Input matching (S11);  $V_{cc} = 5\text{ V}$



a. S22: 40 MHz – 1140 MHz

- (1):  $V_{ctr} = 2.13\text{ V}$
- (2):  $V_{ctr} = 1.80\text{ V}$
- (3):  $V_{ctr} = 1.64\text{ V}$
- (4):  $V_{ctr} = 1.50\text{ V}$
- (5):  $V_{ctr} = 1.39\text{ V}$
- (6):  $V_{ctr} = 1.29\text{ V}$
- (7):  $V_{ctr} = 1.12\text{ V}$

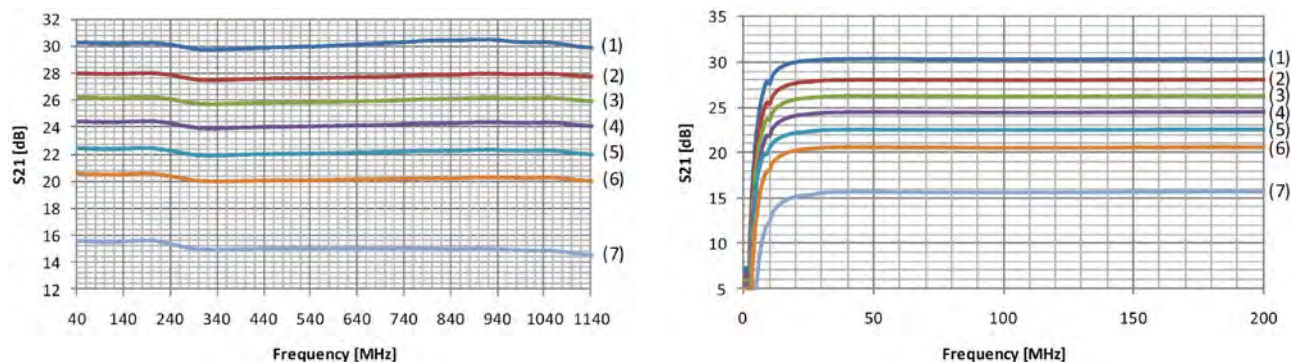


b. S22: 300 kHz – 200 MHz

- (1):  $V_{ctr} = 2.13\text{ V}$
- (2):  $V_{ctr} = 1.80\text{ V}$
- (3):  $V_{ctr} = 1.64\text{ V}$
- (4):  $V_{ctr} = 1.50\text{ V}$
- (5):  $V_{ctr} = 1.39\text{ V}$
- (6):  $V_{ctr} = 1.29\text{ V}$
- (7):  $V_{ctr} = 1.12\text{ V}$

Fig 12. Output matching (S22);  $V_{cc} = 5\text{ V}$





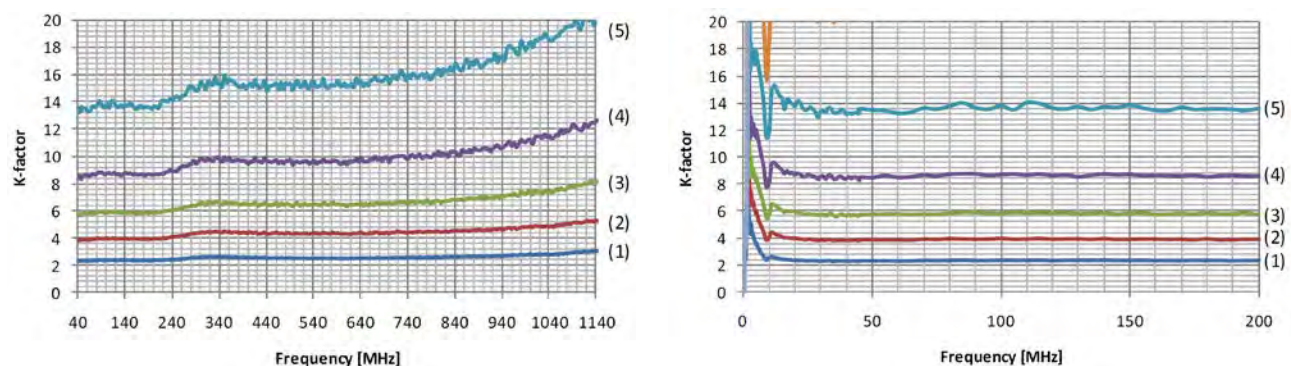
a. S21: 40 MHz – 1140 MHz

- (1): Vctr = 2.13 V
- (2): Vctr = 1.80 V
- (3): Vctr = 1.64 V
- (4): Vctr = 1.50 V
- (5): Vctr = 1.39 V
- (6): Vctr = 1.29 V
- (7): Vctr = 1.12 V

b. S21: 300 kHz – 200 MHz

- (1): Vctr = 2.13 V
- (2): Vctr = 1.80 V
- (3): Vctr = 1.64 V
- (4): Vctr = 1.50 V
- (5): Vctr = 1.39 V
- (6): Vctr = 1.29 V
- (7): Vctr = 1.12 V

Fig 13. Gain (S21); Vcc = 5 V



a. S21: 40 MHz – 1140 MHz

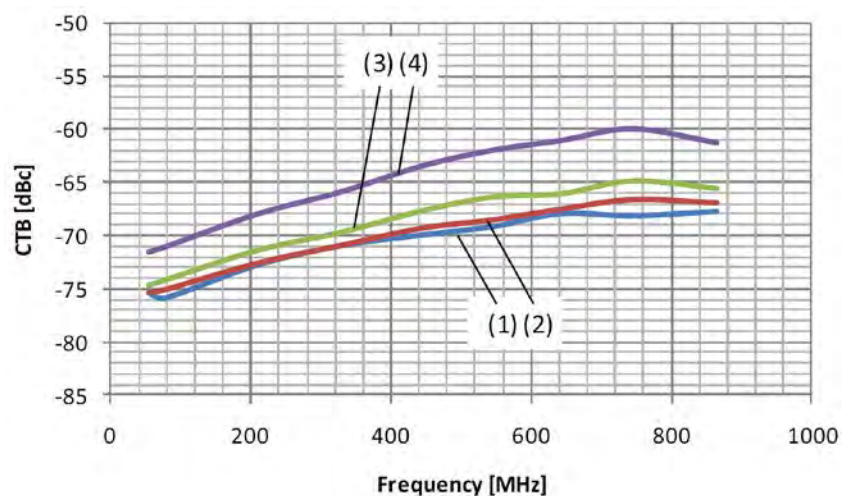
- (1): Vctr = 2.13 V
- (2): Vctr = 1.80 V
- (3): Vctr = 1.64 V
- (4): Vctr = 1.50 V
- (5): Vctr = 1.39 V
- (6): Vctr = 1.29 V
- (7): Vctr = 1.12 V

b. S21: 300 kHz – 200 MHz

- (1): Vctr = 2.13 V
- (2): Vctr = 1.80 V
- (3): Vctr = 1.64 V
- (4): Vctr = 1.50 V
- (5): Vctr = 1.39 V
- (6): Vctr = 1.29 V
- (7): Vctr = 1.12 V

Fig 14. K-factor; typical; Vcc = 5 V

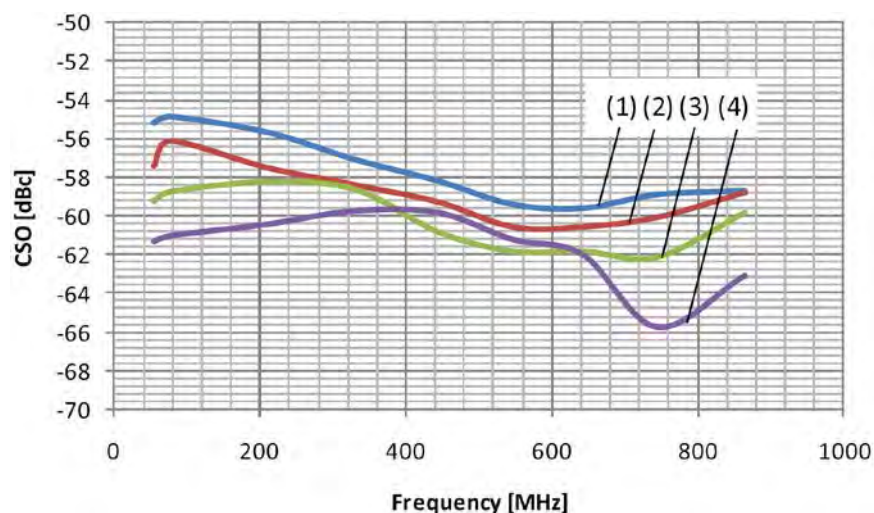
## 6.2 Distortion



- (1):  $V_{ctr} = 2.13 \text{ V}$     (3):  $V_{ctr} = 1.00 \text{ V}$   
 (2):  $V_{ctr} = 1.15 \text{ V}$     (4):  $V_{ctr} = 0.84 \text{ V}$

132 channels NTSC,  $V_o = 30 \text{ dBmV}$

**Fig 15. Composite triple beat (CTB);  $V_{cc} = 5 \text{ V}$**

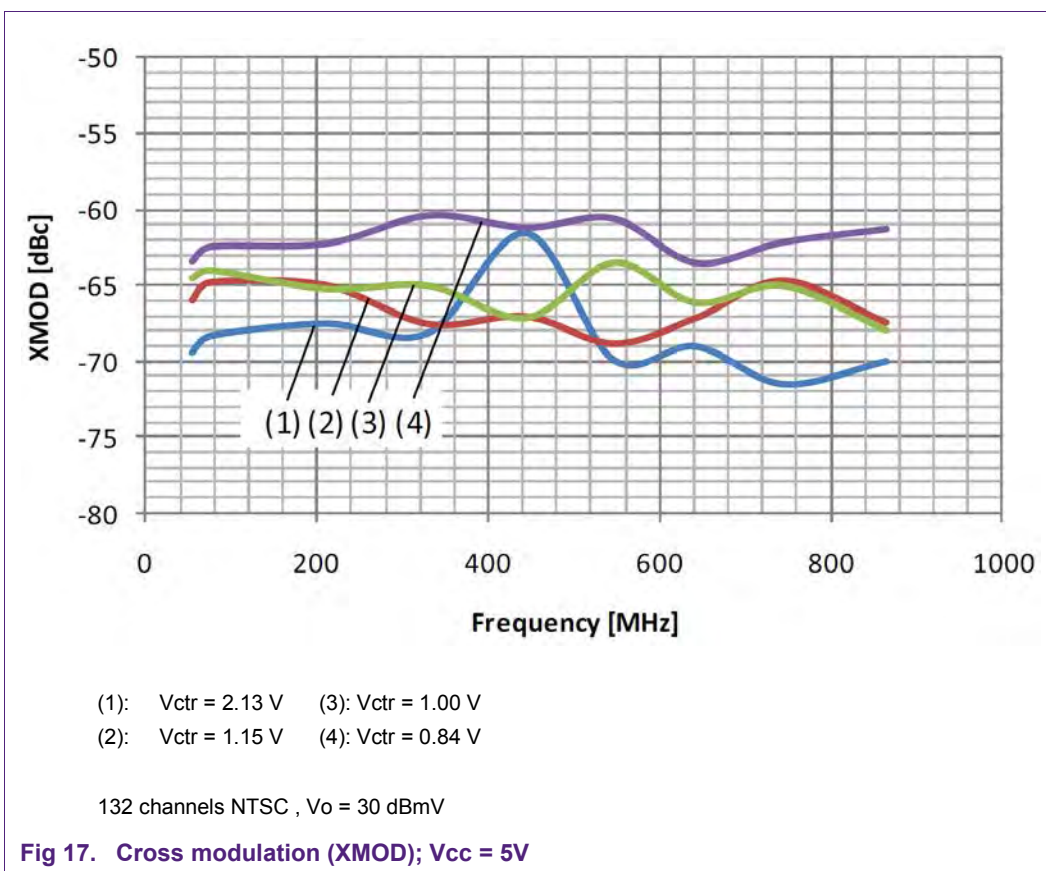


- (1):  $V_{ctr} = 2.13 \text{ V}$     (3):  $V_{ctr} = 1.00 \text{ V}$   
 (2):  $V_{ctr} = 1.15 \text{ V}$     (4):  $V_{ctr} = 0.84 \text{ V}$

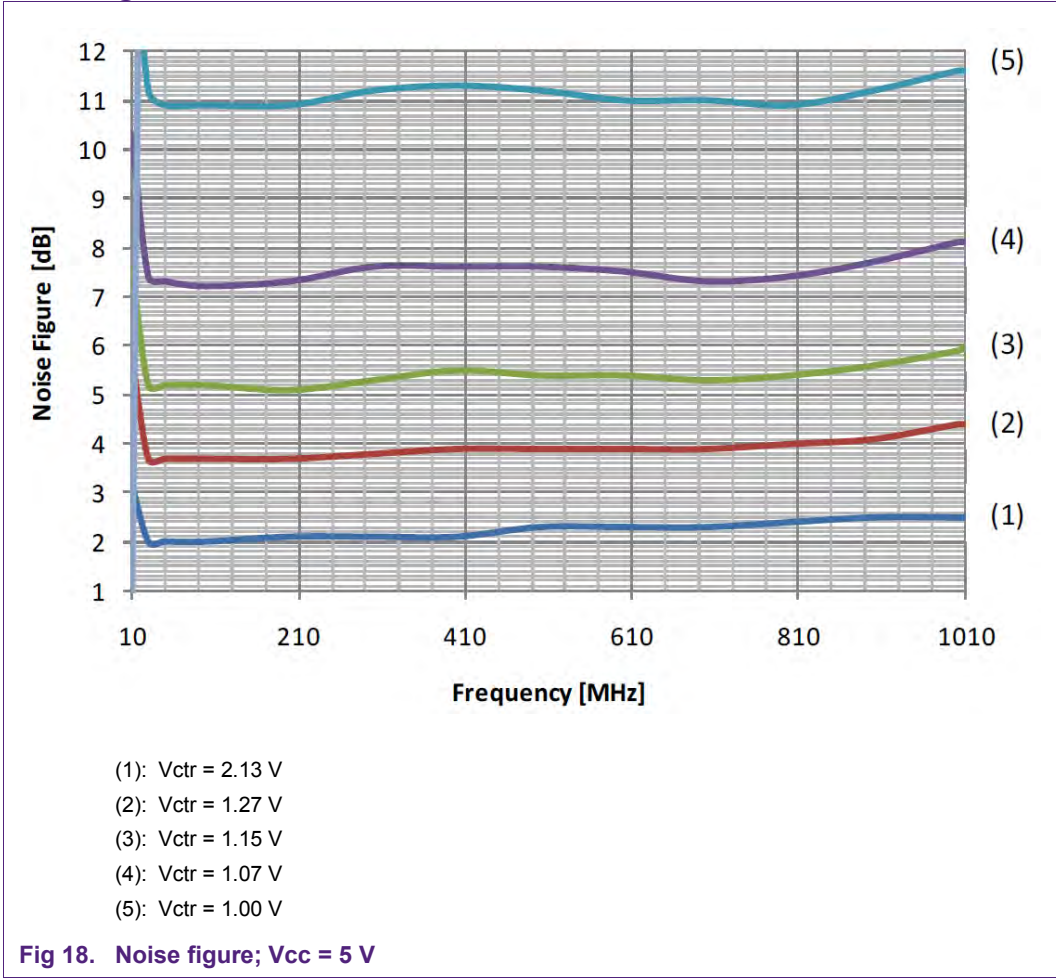
132 channels NTSC,  $V_o = 30 \text{ dBmV}$

**Fig 16. Composite second order (CSO);  $V_{cc} = 5 \text{ V}$**





6.3 Noise figure



## 7. Abbreviations

**Table 2. Abbreviations**

<b>Acronym</b>	<b>Description</b>
AC	Alternating Current
CATV	Community Antenna Television
DC	Direct Current
ESD	Electro Static Discharge
MMIC	Monolithic Microwave Integrated Circuit
PCB	Printed Circuit Board
RF	Radio Frequency
SMD	Surface Mounted Device

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### 8.1 Definitions

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